

Appendix E Noise Technical Report

Noise Technical Report

Final
South Glendale Community Plan

City of Glendale

August 2017

Quality information

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1. Introduction and Objectives

This technical report evaluates potential noise impacts attributed to the proposed South Glendale Community Plan (SGCP) for the community of South Glendale, located south of State Route 134 (SR-134) in Glendale, California (City). This plan serves as long-range guide to development with a focus on the distribution and arrangement of land, roadway and transit networks, and preservation and enhancement of natural open space, historic resources, and cultural resources through the next 25 years. The City intends to rely on the SGCP and associated discretionary actions in their effort to establish neighborhoods, centers, and corridors that the City desires to either maintain, enhance, or transform.

An increase in medium and high-density residential land uses within the SGCP areas would result in the introduction of noise-sensitive receptors in areas that may not have previously been considered noise sensitive. The policies proposed by the plan intend to reflect or enhance applicable noise guidelines in the existing General Plan with a community-specific approach.

Existing noise sources characterizing the SGCP area are dominated by vehicular traffic noise from highways and local roadways, with lesser contributions from passenger rail operation, aircraft overflights, HVAC unit operation, sounds associated with commercial and industrial operations, and intermittent sound sources typical of urban/suburban communities including but not limited to human speech, vehicle idling, car horns, landscaping activity, and amplified music and speech from audio systems in vehicles and homes.

1.1 Community Plan Areas, Goals, and Policies

The SGCP area encompasses roughly 4.6 square miles of land, approximately bounded on the north by SR-134, on the west by the Southern California Regional Rail Authority railroad corridor, variably on the south by several streets, and on the east by State Route 2 (SR-2). The primary goals, recommendations, and objectives of the SGCP include establishment of transit-oriented residential and commercial developments and pedestrian, bicycle, and transit mobility improvements. The community plan area to Maintain, Enhance and Transform are indicated in Figure 4.2-1.

Future development plans for specific projects within the SGCP are not identified or analyzed as part of this technical noise report. However, it is assumed that any such project-specific development plans would undergo a project specific environmental review to identify potential noise and vibration impacts associated with their construction and operation.

2. Fundamentals of Noise and Vibration

2.1 Noise

Noise is generally defined as unwanted or objectionable sound. The effects of noise on people can include general annoyance, interference with speech communication, sleep disturbance and, in the extreme, hearing impairment. The unit of measurement used to describe a noise level is the decibel (dB); decibels are measured on a logarithmic scale that quantifies sound amplitude in a manner similar to the Richter scale used for earthquake magnitudes. Thus, a doubling of the energy of a noise source, such as doubling of traffic volume, would increase the noise level by 3 dB; a halving of the energy would result in a 3-dB decrease.

Human Perception of Noise

The human ear is not equally sensitive to all frequencies within the sound spectrum. Therefore, a method called “A-weighting” is used to filter noise frequencies that are less audible to the human ear. The A scale approximates the frequency response of the average young ear when listening to most ordinary everyday sounds. When people make relative judgments of the loudness or annoyance of a sound, their judgments correlate well with the A-scale levels of those sounds. Therefore, the “A-weighted” noise scale is used for measurements and standards involving the human perception of noise. In this report, all noise levels are A-weighted and “dBA” is understood to identify the A-weighted decibel. Table 2.1-1 Typical Noise Levels provides typical noise levels associated with common activities.

Human perception of noise has no simple correlation with acoustical energy. The perception of noise is not linear in terms of dBA or in terms of acoustical energy. Two noise sources do not sound twice as loud as one source. It is widely accepted that the average healthy ear can barely perceive changes of 3 dBA (increase or decrease); that a change of 5 dBA is readily perceptible; and that an increase (or decrease) of 10 dBA sounds about twice (or half) as loud (Caltrans 2011).

Averaging Noise Levels

In addition to noise levels at any given moment, the duration and averaging of noise over time is also important for the assessment of potential noise disturbance. Noise levels varying over time are averaged over a period of time, usually hour(s), expressed as dBA L_{eq} . For example, L_{eq} (3h) would be a 3-hour equivalent average noise level. When no period is specified, a 1-hour average is assumed (L_{eq} (1h) or L_{eq}).

Common Outdoor Activities	Noise Level (dBA)	Common Indoor Activities
-	110	Rock Band
Jet Fly-over at 300 m (1,000 ft)	100	-
Gas Lawn Mower at 1 m (3 ft)	90	-
Diesel Truck at 15 m (50 ft), at 80 km/hr (50 mph)	80	Food Blender at 1 m (3 ft) Garbage Disposal at 1 m (3 ft)
Noisy Urban Area, Daytime Gas Lawn Mower, 30 m (100 ft)	70	Vacuum Cleaner at 3 m (10 ft)
Commercial Area Heavy Traffic at 90 m (300 ft)	60	Normal Speech at 1 m (3 ft)
Quiet Urban Daytime	50	Large Business Office Dishwasher in Next Room
Quiet Urban Nighttime	40	Theater, Large Conference Room (Background)
Quiet Suburban Nighttime	30	Library
Quiet Rural Nighttime	20	Bedroom at Night, Concert Hall (Background)
-	10	Broadcast/Recording Studio
Lowest Threshold of Human Hearing	0	Lowest Threshold of Human Hearing

Source: Caltrans 2011

Notes: m = meters, ft = feet

km/hr = kilometers per hour

mph = miles per hour

The time of day of noise is also an important factor to consider when assessing potential community noise impacts, as noise levels that may be acceptable during the daytime hours may create disturbance during evening or nighttime hours, when people are typically at home and sleeping. The Community Noise Equivalent Level (CNEL) is a descriptor used to characterize average noise levels over a 24-hour period, calculated from hourly L_{eq} values, with 5 dBA added to the hourly L_{eq} levels occurring between 7:00 p.m. and 10:00 p.m. and 10 dBA added to the hourly L_{eq} levels occurring between 10:00 p.m. and 7:00 a.m., to reflect the greater disturbance potential from evening and nighttime noise, respectively. The day/night average sound level (L_{dn}) is the same as the CNEL, except the evening period is included in the daytime period.

Noise Attenuation

From the source to the receiver, noise changes both in level and frequency spectrum. The most obvious change is the decrease in noise as the distance from the source increases. The manner in which noise reduces with distance depends on the following important factors: ground absorption, atmospheric effects and refraction, shielding by natural and man-made features, noise barriers, diffraction, and reflection. For a point noise source, such as stationary construction equipment, the attenuation rate or drop-off in noise level would be at least -6 dBA for each doubling of unobstructed distance between source and the receiver, and could improve to a rate of -7.5 dBA depending on the

acoustic characteristics of the ground surface over which the sound travels between the source and a receiver. For a linear noise source, such as vehicles traveling on a roadway, the attenuation rate or drop-off in noise level would be approximately -3 dBA for each doubling of unobstructed distance between source and the receiver and could improve up to a rate of -4.5 dBA depending on the acoustic characteristics of the ground surface.

A large object in the path between a noise source and a receiver can significantly attenuate noise levels at that receiver. The amount of attenuation provided by this “shielding” depends on the size of the object and the frequencies of the noise levels. Natural terrain features, such as hills and dense woods, as well as man-made features, such as buildings and walls, can significantly alter noise levels. Walls or berms are often specifically used to reduce noise at one or more receptors with respect to identified substantial sound sources of concern.

Noise Sensitive Receptors

Some land uses are considered more sensitive to noise than others due to the types of activities involved, such as sleeping, reading, talking, or convalescing. Noise-sensitive receptors are generally considered places where humans are engaged in activities, or occupying land uses, that may be subject to the stress or significant interference from noise. Typically, land uses associated with noise-sensitive human receptors include residential dwellings, hotels/motels, hospitals, nursing homes, educational facilities, libraries and recreational facilities, many of which are represented in the SGCP area.

In addition to human receptors, protected animal species and their habitats, e.g., bird species protected under the Migratory Bird Treaty Act, may be considered noise sensitive receptors during their breeding season if they are present in the study area. Temporary, indirect impacts could potentially arise from construction-generated noise resulting in destruction and/or avoidance of habitat by wildlife.

2.2 Vibration

In addition to noise, some construction and transportation activities can generate substantial ground vibration, which can be interpreted as energy transmitted in waves through the soil mass. These energy waves generally dissipate with distance from the vibration source, with propagation distances determined by frequency, frictional losses, and soil types and strata. When groundborne vibrations reach receiving structures, the energy can be transmitted to the foundation of the buildings which in turn may result in vibration of the building structure to varying degrees.

Typical outdoor sources of perceptible groundborne vibration are construction equipment, traffic on rough (i.e., unpaved or uneven) roads and some rail activity. Some construction activity can also result in varying degrees of groundborne vibration, depending on the type of equipment, methods employed, distance between source and receptor, duration, number of perceived vibration events, and local geology.

One major concern with regard to construction vibration is potential building damage, which is assessed in terms of peak particle velocity (PPV) and typically in units of inches per second (in/sec). In addition to structural damage, the groundborne vibration may also induce human annoyance. Human annoyance thresholds are typically much lower than building damage thresholds, both of which are discussed in Section 3.1.3.

3. Noise Analysis Overview

3.1 Regulatory Overview and Impact Criteria

3.1.1 California Code of Regulations

Title 24, Part 2, Chapter 12, Section 1207 covers sound transmission regulations that are applicable to all new construction in the state of California. Section 1207.4 stipulates that interior noise levels generated by exterior noise sources shall not exceed 45 dB CNEL or L_{dn} within a habitable room (whichever noise metric is utilized in the noise element of the local general plan). The City of Glendale General Plan relies upon the CNEL metric for compliance assessment and thus, interior noise levels within habitable spaces as a result from exterior noise sources cannot exceed 45 dBA CNEL. Section 1207.5 directs the reader to the California Green Building Standards Code, Chapter 5, Division 5.5 for additional sound transmission requirements.

3.1.2 California Green (CalGreen) Environmental Comfort

Title 24, Part 11, Section 5.507 specifies environmental comfort with regard to noise exposure for non-residential buildings. The subsections therein provide means of acoustical controls through which building assembly and component requirements are used to assess exterior noise issues. Section 5.507.4 stipulates two compliance approaches. The prescriptive method is utilized when occupied structures are planned with a 65 CNEL contour of an airport, railroad, highway traffic, or industrial noise source. In this case, the wall and roof-ceiling assemblies are required to achieve a composite sound transmission class (STC) rating of at least 50, or a composite outdoor-indoor transmission class (OITC) rating of not less than 40. Additionally, exterior windows are required to be rated with a minimum STC of 40, or OITC of 30. The performance method does not require specific STC and OITC ratings; however, it requires that the interior noise environment attributable to outdoor noise sources not exceed an hourly L_{eq} of 50 dBA. This could be done by means of building envelope construction and/or exterior features such as noise walls or berms. The performance method requires an acoustical analysis documenting compliance with the interior sound level limits, prepared and approved by the architect or engineer of record.

3.1.3 California Department of Transportation (Caltrans) - Vibration

The Caltrans Transportation and Construction Vibration Guidance Manual (Caltrans 2013) (Caltrans Manual) provides guidance for the analysis of vibratory impacts generated by transportation and construction projects. As discussed in the following Section, the City of Glendale relies on human perception to determine violations. The Caltrans Manual identifies the following for “distinctly perceptible” vibration perceptions:

- 0.25 peak particle velocity (PPV) in inches per second (in/sec) for transient sources (sources that induce a single vibratory event, such as blasting); and
- 0.04 PPV in in/sec for continuous or frequent sources (such as pile driving equipment and other construction activities that generate multiple vibration-intensive events across a given period).

Caltrans also has a policy regarding highway noise, but this generally applies to highway capacity improvement projects and therefore would not apply to the SGCP project.

3.1.4 City of Glendale Municipal Code

The City regulates noise through the City’s Municipal Code (GMC), Chapter 8.36 Noise Control, Articles I and II. The following sections of the Ordinance provide sound level limits between adjacent properties, noise insulation standards, and construction noise limits (but typically not public roadways which are generally considered to be part of the ambient noise environment).

The City of Glendale regulates noise limits by assessing the offending noise sources influence on the existing ambient noise environment. In order to assess noise with this approach, the City provides a list of presumed ambient noise levels applicable to varying zone types and times of day which are used to address compliance. This levels, reported in Section 8.36.040 Presumed Noise Standards are listed in Table 3.1-1 below.

Zone	Location	Time Period	5-Minute Average Sound Level (dBA)
Residential (Single Family and Duplex) and Cemetery	Exterior	Daytime	55
		Nighttime	45
Residential (Multifamily, Hotels, Motels, and Transient Lodging)	Exterior	Anytime	60
Central Business District and Commercial	Exterior	Anytime	65
Industrial	Exterior	Anytime	70
Residential (All Residential Zones)	Interior	Daytime	55
		Nighttime	45

Source: Glendale Municipal Code, 1995

A specific definition of daytime periods is not provided in the GMC; however, nighttime periods are defined in Section 8.36.020 as between 10 p.m. and 7 a.m.

As discussed in Section 8.63.030 Decibel Measurement Criteria and Section 8.36.050 Minimum and Maximum Ambient Noise Levels, measured noise exterior or interior levels measured while the offending noise source is active, is compared with these presumed noise standards, as applicable to the receiving land use type. Section 8.36.050 continues to elaborate on the various conditions that affect impact assessment by providing the following assessment scenarios:

- If ambient noise levels measured at the receiver while the offending noise source is inactive are below the applicable presumed noise standard, the resulting 5-minute (or more) Leq of this measurement constitutes the actual ambient noise standard at the receiver, and violations would occur if acoustic contribution from the offending noise source elevated the measured ambient noise level by more than 5 dBA.
- If ambient noise levels measured at the receiver while the offending noise source is inactive are at or above the applicable presumed noise standard, the resulting 5-minute (or more) Leq of this measurement constitutes the actual ambient noise standard at the receiver, and violations would occur if acoustic contribution from the offending noise source elevated the measured ambient noise level by more than 5 dBA. However, the measured ambient noise levels may not exceed the presumed noise standard by 5 dBA. By way of example, if the presumed standard is 45 dBA and the measured ambient is 48 dBA, the resulting violation threshold would be 53 dBA (48 dBA + 5 dBA). However, if the measured ambient was 57 dBA, the resulting violation threshold would be capped at 55 dBA (45 dBA [presumed standard] + 5 dBA [allowable increase due to elevated measured ambient] + 5 dBA [increase leading to violation]).
- In cases where the assessment location occurs at the boundary line between two zones, the arithmetic average of both land use presumed noise standards is used.

Section 8.36.080 Construction on Buildings, Structures and Projects regulates noise produced by construction activities when occurring within 500-feet of any residential land use. Construction activities within this distance are prohibited between the hours of 7 p.m. and 7 a.m. and all day on Sundays and holidays outlined in Chapter 3.08 of the GMC, unless a permit has been granted beforehand from the building official. Permits are not required to perform emergency construction work.

Section 8.36.140 Proposed Development Project allows the City's director of community development or the building official to require an acoustic analysis as a condition of approval as a part of the building permit process or other approval procedures either has reason to believe that a new development project, addition, modification, or any other changes thereto would not conform with the permitted noise level standards.

Section 8.36.210 Vibration prohibits the operation or permission of operation of any device that creates vibration in excess of the perception threshold of an individual at or beyond the source property boundary if the source is located on private property, or if it exceeds the perception threshold of an individual at one hundred and fifty feet from the source within a public space or public right-of-way.

Section 8.36.290 Exemptions contains a list of activities that are exempted from the provisions of Chapter 8.36 of the GMC. List item "K" exempts any activity, operation, or noise which cannot feasibly be brought into compliance when it is technically infeasible to do so. The party responsible for the exceedance is also responsible to prove that compliance cannot not be achieved despite use of mufflers, shields, sound barriers, and/or any other noise reduction device or techniques during the operation of the offending equipment.

3.1.5 City of Glendale General Plan

The Noise Element of the City's General Plan (City of Glendale 2007) provides a comprehensive program for noise management during the planning process. The General Plan outlines goals and policies to achieve and maintain land uses that are compatible with environmental noise levels.

The City uses the Noise/Land Use Compatibility Table shown below in Table 3.1-2 for evaluating land use noise compatibility for proposed developments.

Land Use Category	Community Noise Exposure <i>L_{dn}</i> or CNEL, dB						INTERPRETATION
	55	60	65	70	75	80	
Residential - Low Density Single Family, duplex, Mobile Homes	Green		Yellow		Blue		<p>Normally Acceptable Specified land use is satisfactory, based upon the assumption that any buildings involved are of normal, conventional construction, without any special noise insulation requirements.</p> <p>Conditionally Acceptable New construction or development should be undertaken only after a detailed analysis of the noise reduction requirements is made and needed noise insulation features included in the design. Conventional construction, but with closed windows and fresh air supply systems or air conditioning will normally suffice.</p> <p>Normally Unacceptable New construction or development should generally be discouraged. If new construction or development does proceed, a detailed analysis of the noise reduction requirements must be made and needed noise insulation features included in the design.</p> <p>Clearly Unacceptable New construction or development should generally not be undertaken.</p>
Residential - Multi-Family	Green		Yellow		Blue		
Transient Lodging - Motels, Hotels	Green		Yellow		Blue		
Schools, Libraries, Churches, Hospitals, Nursing Homes	Green		Yellow		Blue		
Auditoriums, Concert Halls, Amphiteaters	Yellow		Yellow		Blue		
Sports Area, Outdoor Spectator Sports	Yellow		Yellow		Blue		
Playgrounds, Neighborhood Parks	Green		Yellow		Blue		
Golf Courses, Riding Stables, Water Recreation, Cemeteries	Green		Yellow		Blue		
Office Buildings, Business Commercial and Professional	Green		Yellow		Blue		
Industrial, Manufacturing, Utilities, Agriculture	Green		Yellow		Blue		

Source: City of Glendale 2007

As Table 3.1-2 indicates, the City’s exterior “acceptable” noise level standard for residential uses (single and multiple dwelling units) is 60 dBA *L_{dn}*/CNEL or less for low density residential (single family, duplex, mobile homes) and 65 dBA *L_{dn}*/CNEL for Multi-family residential, hotel/motels, schools, libraries, churches and hospitals. “Conditionally Acceptable” noise exposures for land use indicates that standard construction methods will attenuate exterior noise to an acceptable indoor noise level and people can carry out outdoor activities with minimal noise interference. Residential land uses with exterior noise levels of up to 70 dBA *L_{dn}*/CNEL would require a detailed analysis of the noise reduction requirements and subsequent implementation of necessary noise insulation features in the development design to achieve the City interior noise standard of 45 dBA CNEL. For “normally unacceptable” land uses, new construction and development is discouraged, however, it may be allowed provided that a detailed analysis of the noise reduction requirements is made and subsequent implementation of necessary noise insulation features are included in the design to achieve interior noise standards.

For residential land uses, the “clearly unacceptable” noise level standard is greater than 75 dBA *L_{dn}*/CNEL, and new construction should generally not be undertaken. Outdoor activities would be exposed to severe and unacceptable noise interference, and structures would require extensive mitigation techniques to make the indoor environment acceptable.

General Plan Policy 3.1 ensures that the aforementioned acoustic studies would be prepared by a qualified consultant who would propose conditionals of approval or mitigation measures in order to achieve compliance with the interior and exterior noise standards when future development is proposed in areas exposed to levels greater than 65 dBA CNEL. General Plan Policy 3.2 restates the City’s commitment to enforcing interior noise level standards stipulated by the California Building Code (Title 24, Part 2, Chapter 12, Section 1207).

3.2 Thresholds of Significance

The City of Glendale determines impacts related to noise and vibration using the State California Environmental Quality Act (CEQA). Per CEQA Guidelines Appendix G (as listed for Noise), the Project would be considered as having a significant impact if it resulted in:

- Exposure of persons to or generation of noise levels in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies
- Exposure of persons to or generation of excessive groundborne vibration or groundborne noise levels
- A substantial permanent increase in ambient noise levels in the project vicinity above levels existing without the project
- A substantial temporary or periodic increase in ambient noise levels in the project vicinity above levels existing without the project
- For a project located within an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, exposure of people residing or working in the project area to excessive noise levels
- For a project within the vicinity of a private airstrip, exposure of people residing or working in the project area to excessive noise levels

4. Existing Conditions

4.1 Existing Land Use and Zoning

South Glendale is a highly-developed area with mixture of land uses including single-family and multi-family residential, industrial, commercial retail, office space, and a transportation center. Residential uses comprise the majority of developed land in the SGCP area and are generally located throughout the vicinity.

4.2 Existing Noise Levels

Ambient noise levels were measured within the SGCP area to characterize the existing sound environments and assist in determining constraints and opportunities.

4.2.1 Baseline Ambient Noise Survey

After a preliminary review of online aerial imagery, the draft community plan, and input from City staff, multiple field noise survey location candidates were identified in the SGCP area for short-term (ST) Sound Pressure Level (SPL) measurements. ST measurements were conducted on July 18th, 2017. As depicted in Figure 4.2-1, a total of 8 measurement locations took place within the SGCP area. All ST measurements were conducted in the attendance of the sound level meter (SLM) operator, who made simultaneous documentation of observations (e.g., perceived sound sources and environmental conditions).

4.2.1.1 Instrumentation

The ST measurements were conducted using a Larson-Davis (LD) Model LxT (serial number [SN] 4485) SLM, rated by the American National Standards Institute (ANSI) as Type 1 per IEC 61672-1:2013, ANSI S1.4, and ANSI S1.43. The SLM microphone was fitted with standard 3.5-inch diameter spherical-shaped open-cell foam windscreen and positioned roughly 5 feet above grade. The microphone was also placed at least 10 feet from any vertical acoustically reflecting surfaces. The SLM was set using slow time-response and the A-weighting scale. SLM calibration was field-checked before and after each measurement period with an L/D Model CAL200 (SN 5768) acoustic calibrator. Where not already described, sound level measurements performed for this field survey were conducted in accordance with applicable portions of International Organization for Standardization (ISO) (1996 parts 1, 2, and 3.) standards. A Kestrel Model 3500 (SN 2058303) handheld anemometer was used to determine average wind speed, temperature, barometric pressure, and relative humidity before each round of community measurements.

Measurement ST1 was conducted in the southeastern parking lot of the Larry Zarian Transportation Center, approximately 130 feet from the nearest railroad track, 180 feet from Gardena Avenue edge of pavement (EOP), and 35 feet from the abutting parcel to the southeast. The primary noise source at this location was vehicular traffic on Glendale Avenue. Additional noise sources included train horn soundings, train pass-bys, speech from Larry Zarian Transportation Center visitors, fixed-wing aircraft flyovers, and HVAC operation to the southeast.

Measurement ST2 was conducted in a retail development parking lot on the northeast corner of the South Central Avenue and West Windsor Road intersection. The primary noise source at this location was vehicular traffic on South Central Avenue. Additional noise sources included distant train horn soundings, HVAC, and speech from parking lot activities.

Measurement ST3 was conducted in front of a large warehouse facility located at 4484 San Fernando Road, approximately 30 feet from the San Fernando Road EOP and 140 feet from the nearest railroad track. The primary source of noise at this location was vehicular traffic from San Fernando Road. Additional sources included occasional mechanical noise emanating from within the open-door warehouse facility.

Measurement ST4 was conducted in the large parking area located on the northeast corner of the Pioneer Drive and North Pacific Avenue intersection, immediately south of the SR-134 mainline and westbound (WB) SR-134 on-ramp from North Pacific Avenue. The measurement was located approximately 100 feet south of the aforementioned on-ramp EOP and 180 feet west of the North Pacific Avenue EOP. An existing noise barrier along the SR-134 WB ramp begins approximately 245 feet from the North Pacific Avenue EOP, thus, this measurement location is representative of unmitigated traffic noise levels currently experienced by this currently non-noise sensitive land use. The primary source of noise at this location was highway traffic on SR-134. Additional noise sources included traffic noise contributions from North Pacific Avenue and intermittent fixed-wing aircraft flyovers.

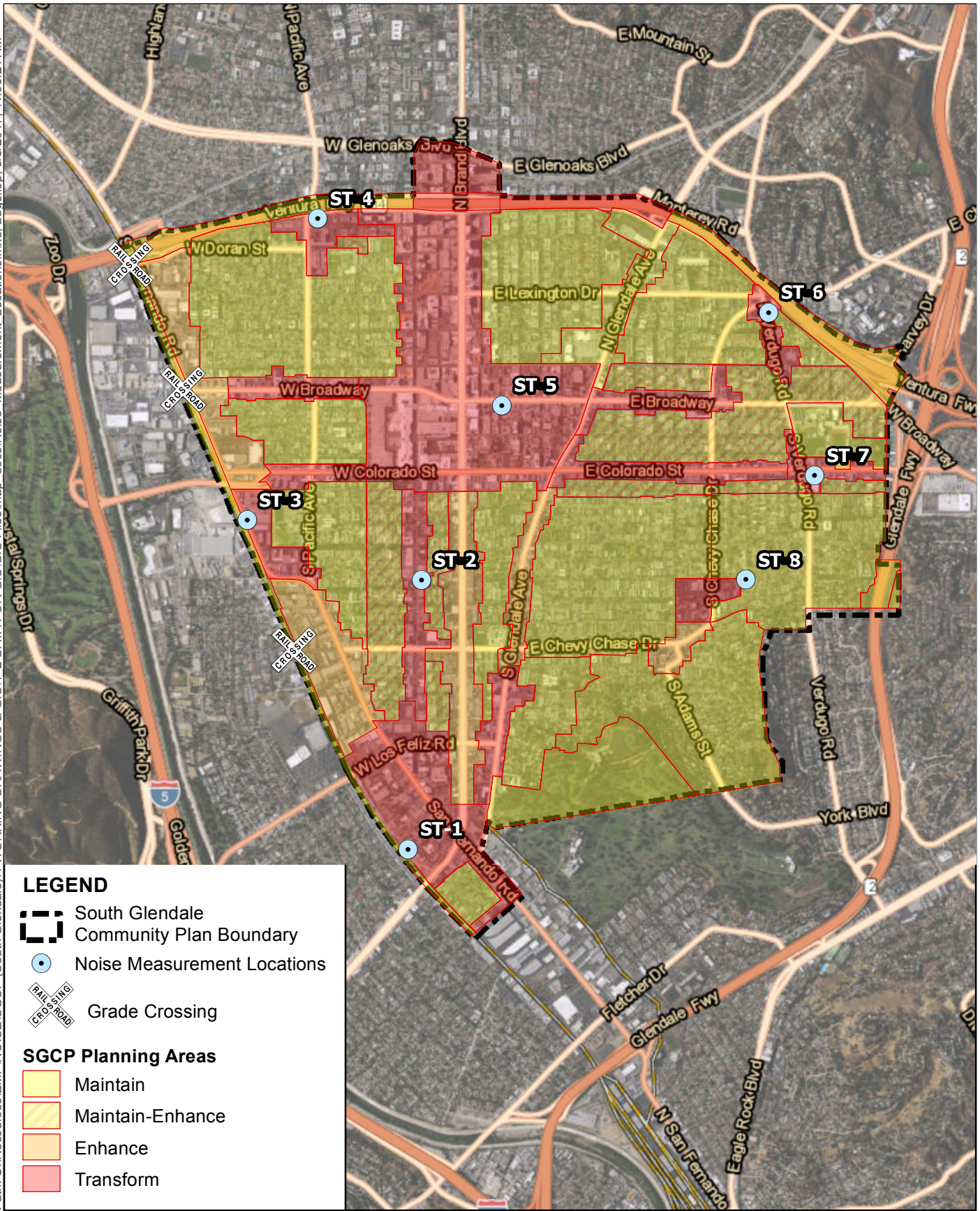
Measurement ST5 was conducted in a parking area on the southeast corner of the South Louise Street and East Broadway intersection, located approximately 18 feet from the EOP of South Louise Street and 85 feet from the East Broadway EOP. The primary noise source at this location was vehicular traffic from East Broadway and South Louise Street. Additional noise sources included dogs barking, radio-communications from construction workers north of the measurement location, and speech from parking lot activities.

Measurement ST6 was conducted in a parking area associated with 320 North Verdugo Avenue, approximately 40 feet from the EOP of North Verdugo Avenue and 158 feet from the EOP of North Chevy Chase Drive. The primary noise source at this location was vehicular traffic from North Verdugo Road. Additional noise sources included traffic from SR-2 and North Chevy Chase Drive, rustling leaves, and birdcalls.

Measurement ST7 was conducted within a parking lot associated with 1416 East Colorado St on the southeast corner of the intersection of Colorado Street and South Verdugo Road, approximately 90 feet from the EOP of Colorado Street and 190 feet from the EOP of Verdugo Road. The primary noise source at this location was traffic on Colorado Street and South Verdugo Road. Additional noise sources included typical parking lot sounds associated with the adjacent grocery store including speech, grocery cart rolling, and vehicle doors and trunks being shut.

Measurement ST8 was conducted at the Windsor Mini Park at the southeast corner of Porter Street and East Windsor Road, approximately 20 feet from the EOP of East Windsor Road and 90 feet from the EOP of Porter Street. The primary noise sources at this location were operating HVAC systems at the apartments on Windsor Road. Additional noise sources included intermittent traffic on East Windsor Road and Porter Street, rustling leaves, birdcalls, children playing, and dogs barking.

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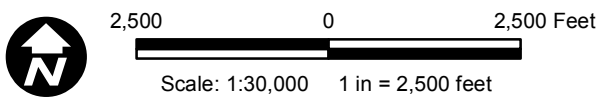
- South Glendale Community Plan Boundary
- Noise Measurement Locations
- Grade Crossing

SGCP Planning Areas

- Maintain
- Maintain-Enhance
- Enhance
- Transform

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**FIGURE 4.2-1
NOISE MEASUREMENT LOCATIONS
AND SGCP PLANNING AREAS**



Results from the short-term measurement survey are provided below in Table 4.2-1. ST measurements durations were 15-minutes, thus, the 15-minute average Leq level is presented as the primary noise level metric. The presented data is not intended for compliance assessment with City's zone-specific 24-hour CNEL compatibility thresholds, but rather to provide insight into existing neighborhood-specific daytime noise levels and the character of the existing noise sources listed in the detailed descriptions.

Table 4.2 1
Existing Community Noise Measurement Results

Meas. ID	Date	Start Time (hh:mm)	Duration (Minutes)	Leq	L _{min}	L _{max}	L ₁₀	L ₅₀	L ₉₀
ST1	7/18/17	09:23	15	60.7	45.3	78.3	57.8	53.1	51.2
ST2	7/18/17	10:09	15	57.5	50.0	72.8	59.5	55.8	52.7
ST3	7/18/17	10:41	15	70.2	53.0	82.3	73.5	68.8	60.2
ST4	7/18/17	11:11	15	64.7	60.2	77.1	66.4	63.3	61.9
ST5	7/18/17	12:04	15	59.4	50.5	73.7	61.3	58.2	54.8
ST6	7/18/17	15:17	15	66.3	54.1	88.2	66.3	60.3	56.9
ST7	7/18/17	14:44	15	60.0	55.0	74.0	61.2	58.7	57.3
ST8	7/18/17	14:16	15	54.7	46.9	69.3	56.2	50.9	49.1

4.2.2 Existing Traffic Noise

Vehicles traveling on SR-134 and SR-2 dominate the existing ambient environment around the northern and eastern boundary of the SGCP area, further supplemented by arterial roadways such as San Fernando Road and Colorado Street. As shown in Table 4.2-1, measured existing noise levels in the SGCP area ranged from 55 to 70 dBA. Since the field observations made during these measurements listed vehicular traffic noise as the primary noise source, these levels are considered representative of existing traffic noise contributions at the eight discrete measurement locations. The majority of noise sensitive receivers located adjacent to the SR-2 and SR-134 right-of-way are currently benefitting from existing traffic noise barriers constructed in varying heights and points along the freeways.

4.2.3 Existing Rail Traffic Noise

Railway noise is generated from the rail traffic on the rail corridor that outlines the western boundary of the SGCP area. This corridor consists of freight operations and regional passenger rail operations (Amtrak and Metrolink). Noise associated with these operations includes locomotive engines, wheel-to-rail and switch noise, horn sounding, station approach and disembark bell sounding, emergency signaling devices, and stationary bells associated with the at-grade crossings at Chevy Chase Drive, West Broadway, and Doran Street. Also located within this corridor is the Larry Zarian Transportation Center, which serves as a stop for Metrolink commuter and Amtrak passenger trains on the corridor, with exception of certain express rail services. Passenger rail movements occur through the SGCP area multiple times per hour between 5 a.m. and 11 p.m. every day. Freight trains also operate along the corridor daily. Rail traffic noise levels greater than or equal to 60 dBA L_{dn} (metric used by the Federal Railroad Administration [FRA]), extend into the SGCP area from the railroad alignment at a distance of approximately 180 feet. Within a 700-foot distance of the three at-grade crossings, noise levels generated by horn soundings will extend the 60 dBA L_{dn} distance to approximately 1060 feet.

4.2.4 Existing Aircraft Noise

The SGCP area experiences regular audible aircraft overflights from small propeller aircraft, jet aircrafts, and intermittently from helicopters. The nearest public or private airport, Hollywood Burbank Airport, is located approximately 5.1 miles northwest of the study area. The Los Angeles County Airport Land Use Plan (Los Angeles 1991) does not include the SGCP area within any airport's Planning Boundary/Airport Influence Area. While aircraft are occasionally audible it is unlikely that they are making quantifiable contribution to the CNEL level in the SGCP area.

4.2.5 Existing Stationary Noise

Ambient noise levels throughout the SGCP areas are typically dominated by surface transportation sources, but local stationary noise sources may also contribute to ambient noise levels in some locations. Stationary noise sources in the SGCP area are generally characterized by the specific land uses. Existing residential areas experience noise sources from stationary noise sources typical of an urban environment, including HVAC operation from nearby residential and non-residential land uses, landscaping, dogs barking, vehicle idling, children playing, and operating entertainment systems with loudspeakers.

5. Noise Analysis Methodology

5.1 Surface Transportation

5.1.1 Roadway Traffic

Existing and future traffic noise levels were predicted using the FHWA Traffic Noise Model (TNM) Version 2.5, the most recent version approved by the FHWA at the time of this analysis. This screening-level noise analysis considered the following TNM input parameters: traffic mix, vehicle speed, traffic volume, and roadway-specific paved width. While the model has the capability to account for roadway gradients, and shielding effects from terrain and buildings/barriers, this analysis assumed flat topography throughout SGCP area and omitted existing structures that may offer additional shielding to noise sensitive land uses. However, it is noted that highway noise barriers do exist on many of the sections of SR-134 that are adjacent to residential neighborhoods in the SGCP area, so predicted noise contours in these areas would be particularly conservative (residential receptors located immediately behind freeway noise barriers typically receive a 5 to 10 dBA noise reduction).

Existing (2017) and future (2040) traffic volumes for the local roadways were provided by consulting firm Fehr & Peers in conjunction with their South Glendale Community Plan Transportation Analysis Report (Fehr & Peers 2017). The heavy truck and medium truck mixes for local roadways were determined by traffic observations made during the existing ambient noise measurement survey. On these local roadways, modeled truck percentages ranged from 2-3%. The truck mixes for freeways were calculated from traffic quantities on aerial imagery, resulting in a 3% medium and heavy truck mix for SR-134, and 4% medium truck and 1% heavy truck ratio on SR-2.

Traffic counts provided by Fehr & Peers included existing and future traffic volumes at an hourly resolution, allowing for precise calculation of specific traffic volumes across the daytime, evening, and nighttime time periods. Using an array of modeled receiver locations at varying distances from the edge-of-pavement of each modeled roadway in TNM, L_{eq} values were calculated at pertinent distances and subsequent converted into CNEL values for report tables and for use in the generation of figures displaying isopleths or contour buffers of applicable CNEL values. Attachment C displays detailed traffic information used for modeling all roadway segments, including speed limits, roadway paved widths, existing and future time period-specific ADTs, and truck traffic percentage mixes.

5.1.2 Rail Noise

Noise generated by railroad operations was modeled following recommendations in the FTA-recommended Noise Impact Assessment Spreadsheet (Harris Miller Miller & Hanson, Inc. 2007). Input parameters used in these analyses included train type, frequency of pass-bys during daytime (7 a.m. – 10 p.m.) and nighttime (10 p.m. and 7 a.m.) hours, speed of travel, and total number of rail cars. The Noise Impact Assessment Spreadsheet has a calculation output of a day-night noise levels (L_{dn}), although this is calculated differently from CNEL values. L_{dn} values are typically always within 1 dBA of CNEL values; thus, this analysis considers the L_{dn} output of the Impact Assessment Spreadsheet to be analogous to the CNEL values required for land use planning and noise assessment.

Both passenger and freight rail speeds through the SGCP area were modeled to be traveling at speeds of 30 miles per hour (mph) through the majority of the area, with exception for rail segments near the Larry Zarian Transportation Center, where modeled passenger rail speeds were reduced to 15 mph. Passenger trains were modeled with a single locomotive engine, while freight trains were assumed to have an average of three. Input parameters for daytime/nighttime pass-by frequencies were obtained from published Amtrak and Metrolink timetables, details from which are shown below in Table 5.1-1.

Freight train schedules are not standardized or publicly available. Thus, this analysis used assumptions made in the Technical Appendix to the City of Glendale Noise Element of the General Plan (Mestre Greve Associates 2005), which, from discussions with Union Pacific representatives and on-site observations, estimated an average of 10 freight train pass-bys each day. With no additional available information on specific schedules, this study interprets “each day” to mean during daytime hours; However, this study assumes that at least one freight train will operate along this track between the nighttime hours of 10 p.m. and 7 a.m., to provide for a worst case analysis.

**Table 5.1 1
Passenger Rail Operations Assumptions**

Train Service	Typical Locomotives / Cars Per Train	Quantity per Time Frame		Modeled Speed (mph)
		Daytime (7 a.m. to 10 p.m.)	Nighttime (10 p.m. to 7 a.m.)	
Metrolink	1 / 5	56	7	30 / 15
Amtrak	1 / 6	12	0	30
Freight	3 / 80	9	1	30

Sources: Metrolink 2017, Amtrak 2017

Due to the presence of roadway grade crossings, train horn sounding was modeled at grade crossings as required by the Code of Federal Regulations (CFR) 49 CFR Part 222 Use of Locomotive Horns at Public Highway-Rail Grade Crossings. As stipulated in 49 CFR Part 222, when trains are traveling below 60 miles-per-hour, locomotive horns are required to be sounded no sooner than 15 seconds and no later than 20 seconds before the locomotive enters the crossing. Thus, at a modeled speed of 30 miles-per-hour at the crossings, or 44 feet-per-second, train horn soundings were modeled to occur at the 17-second approach mark, or, approximately 750 feet from either side of the grade crossing.

Additional details regarding input parameters for the Impact Assessment Spreadsheet are included in Attachment B.

6. Future Noise Environment and Impacts

6.1 Exposure of persons to or generation of noise levels in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies

6.1.1 Vehicular Noise

The vehicular traffic from adjacent freeways is the dominant noise source affecting land use compatibility within the SGCP area. The distances to the 60 dBA, 65 dBA, 70 dBA, and 75 dBA CNEL noise contours attributed to traffic volumes attributed to growth and implementation of the community plan are shown in Table 6.1-1. Distances to the roadway noise contours are based on an assumed hard, flat site, with no intervening barriers or obstructions. Existing and Future year noise contours for the proposed SGCP area are shown graphically, together with contributions from predicted existing and future rail noise, in Figures 6.1-1 and 6.1-2, respectively.

Table 6.1 1
Future Vehicle Traffic Noise CNEL Contour Distances for the
South Glendale Community Plan Area

Roadway	Modeled Roadway Segment	Distance to Predicted dBA CNEL (Approximate Feet from Roadway Edge of Pavement)			
		75	70	65	60
Brand Boulevard	North of Lexington Drive	<1	<1	53	190
	North of Broadway	<1	<1	42	168
	North of Colorado St	<1	<1	46	176
	North of Chevy Chase Drive	<1	<1	36	155
	North of Los Feliz Road	<1	<1	42	169
	North of San Fernando Road	<1	<1	43	174
Broadway	East of San Fernando Road	<1	<1	20	97
	East of Pacific Avenue	<1	4	51	160
	East of Brand Boulevard	<1	4	53	163
	East of Glendale Avenue	<1	9	66	182
	East of Verdugo Road	<1	17	88	206
Chevy Chase Drive	East of San Fernando Road	<1	3	50	159
	East of Brand Boulevard	<1	14	81	198
	East of Glendale Avenue	<1	14	81	199
	North of Acacia Avenue	<1	<1	16	91
	North of Colorado St	<1	<1	40	150
	North of Broadway	<1	<1	30	126
Colorado Street	East of San Fernando Road	<1	<1	31	127
	East of Pacific Avenue	<1	25	121	279
	East of Brand Boulevard	<1	23	110	246
	East of Glendale Avenue	<1	19	100	237
	East of Verdugo Road	<1	17	93	231
Glendale Avenue	North of Lexington Drive	<1	10	83	236
	North of Broadway	<1	2	60	196
	North of Colorado St	<1	4	64	206
	North of Chevy Chase Drive	<1	2	53	178
	North of Los Feliz Road	<1	5	62	194
	North of San Fernando Road	<1	4	52	163
Pacific Avenue	North of Lexington Drive	<1	12	75	192
	North of Broadway	<1	7	59	173
	North of Colorado St	<1	9	65	181
	North of San Fernando Road	<1	<1	18	91
San Fernando Road	North of Broadway	<1	14	88	225
	North of Colorado St	<1	12	83	220
	North of Chevy Chase Drive	6	44	119	197
	North of Los Feliz Road	<1	24	115	265
	East of Brand Boulevard	<1	38	148	296
York Boulevard / South Adams Street	East of Verdugo Road	<1	<1	19	86
Freeways					
State Route 134	At Pacific Avenue	358	613	865	1211
	At Central Avenue / Brand Blvd	361	614	864	1214
	At Glendale Avenue	380	627	883	1239
State Route 2	At York Boulevard / Delevan	264	594	870	1212

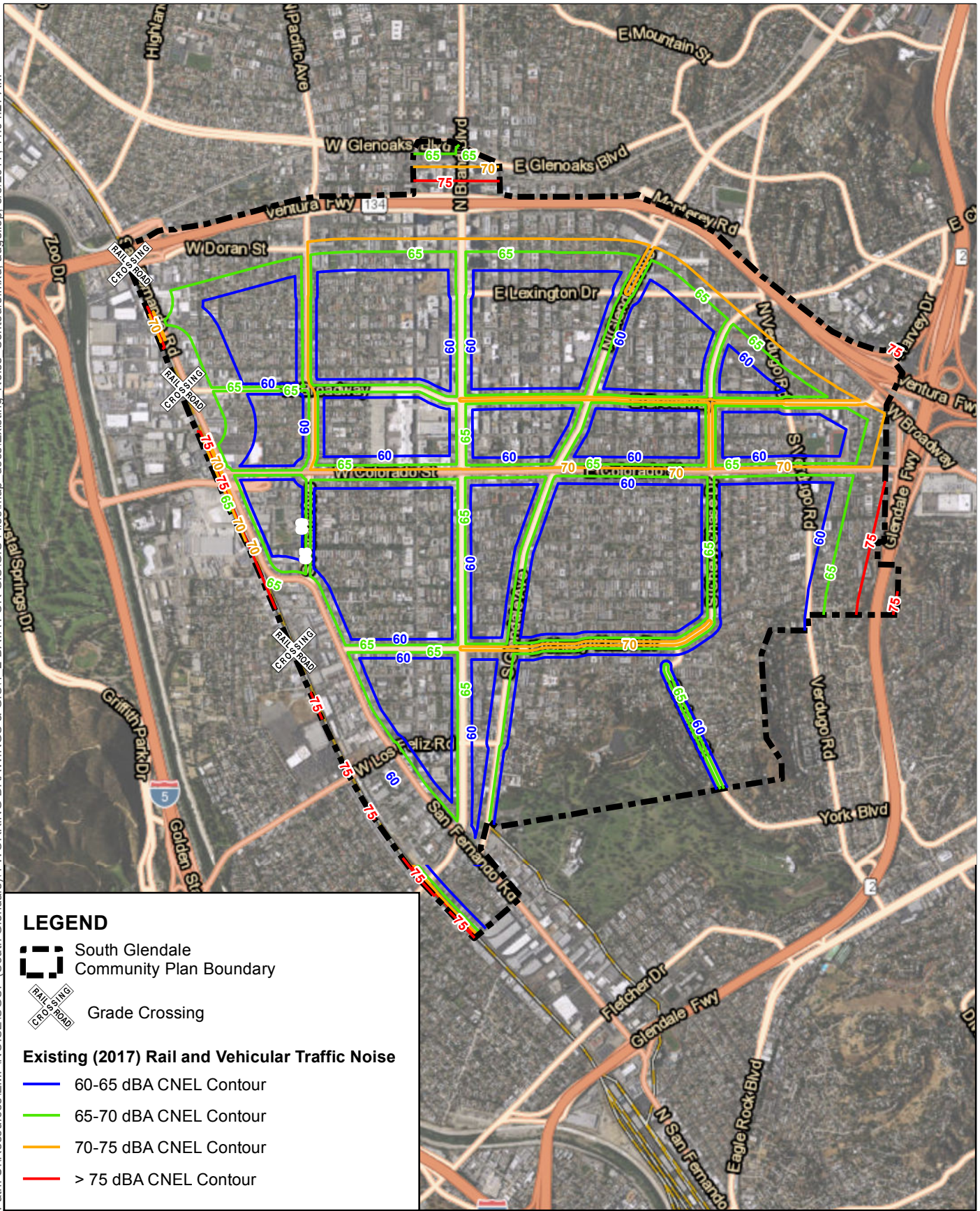
At any specific noise sensitive land use, the actual existing noise levels would depend upon not only the current source noise level, but also the nature of the path of sound from the source to the receptor. In many cases, structures, ground topography, and other obstacles obstruct the direct line of sight from receptor to the traffic noise sources, which could significantly reduce noise exposure at discrete receptor locations.

Shown in Figure 6.1-1 and 6.1-2, are existing and future combined traffic and rail noise levels contours within the proposed SGCP area (more information on rail noise predictions Section 6.1.2). In several areas it appears that existing and proposed residential use areas would, in cases of residences close to the freeways and major roadways, exceed the General Plan Noise Element “conditionally acceptable” thresholds for residential land uses (70 dBA CNEL) for both existing and future conditions. Noise levels greater than 75 dBA CNEL are considered “clearly unacceptable” for residential land uses, but may be allowed under certain conditions for land uses such as business commercial, industrial, and other non-noise-sensitive land uses. Land uses located adjacent to SR-134 and SR-2 have the potential to be exposed to noise levels greater than 75 dBA CNEL in areas where existing noise barriers are not currently constructed. Broader mitigation for proposed development, such as additional noise barriers adjacent to freeways and roadways, can reduce exterior noise to levels compliant with General Plan Noise Element guidelines.

In the SGCP area, future noise levels for residential land uses would be “clearly unacceptable” (i.e., greater than 75 dBA CNEL) at areas located within approximately 358 to 380 feet from the SR-134 EOP and 264 feet from the SR-2 EOP, and normally unacceptable (i.e., greater than 70 dBA CNEL) at areas located within approximately 613 to 637 feet from the SR-134 EOP and 594 feet from the SR-2 EOP. These areas are currently developed; however, the proposed SGCP and associated discretionary actions would result in changes to the land use in these areas, including the introduction of new sensitive land uses. The development of new noise-sensitive land uses proposed in the SGCP may subject receptors to noise levels that exceed General Plan guidelines in vicinities not shielded by existing highway noise barriers. The plan proposes to transform neighborhoods within these areas, such as those located in the immediate vicinity of the freeways in the Tropico, Pacific Edison Center, Pacific Avenue Gateway, Downtown, Verdugo Road, and East Colorado Gateway areas, all have potential to experience CNEL levels greater than 75 dBA. Per Table 2 of the General Plan Noise Element, any future residential use in areas experiencing noise levels above 65 dBA CNEL would be required to meet exterior and interior noise standards applicable to the proposed land use category by means of both exterior and interior noise attenuation measures.

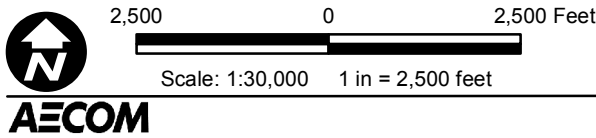
Policies in the proposed SGCP, General Plan, and California Building Code would reduce traffic noise exposure because they set standards for the siting of noise sensitive land uses. Noise Element Policy 3.1 requires a noise study prepared by qualified consultants for new land use, as described in the Land Use column of Table 2 of the Noise Element in areas where the existing or future noise levels exceed or would exceed the “acceptable” noise level thresholds. Site-specific exterior noise analyses that demonstrate that the project would not place sensitive receptors in locations where the exterior existing or future noise levels would exceed the noise compatibility guidelines of the General Plan would be required as part of future discretionary proposals. Site-specific interior noise studies demonstrating compliance with the interior noise compatibility guidelines of the General Plan would also be required for land uses located in areas where exterior noise levels exceed the noise and land use compatibility thresholds as defined in the General Plan, and Noise Element Policy 3.2 requires continued enforcement of California Building Code (Title 24 Compliance Reports) to demonstrate that the building envelope acoustic performance results in interior noise levels of 45 dBA CNEL or less. With this framework, exterior traffic noise impacts associated with new development requiring discretionary approvals and interior traffic noise impacts for both ministerial and discretionary projects would be less than significant.

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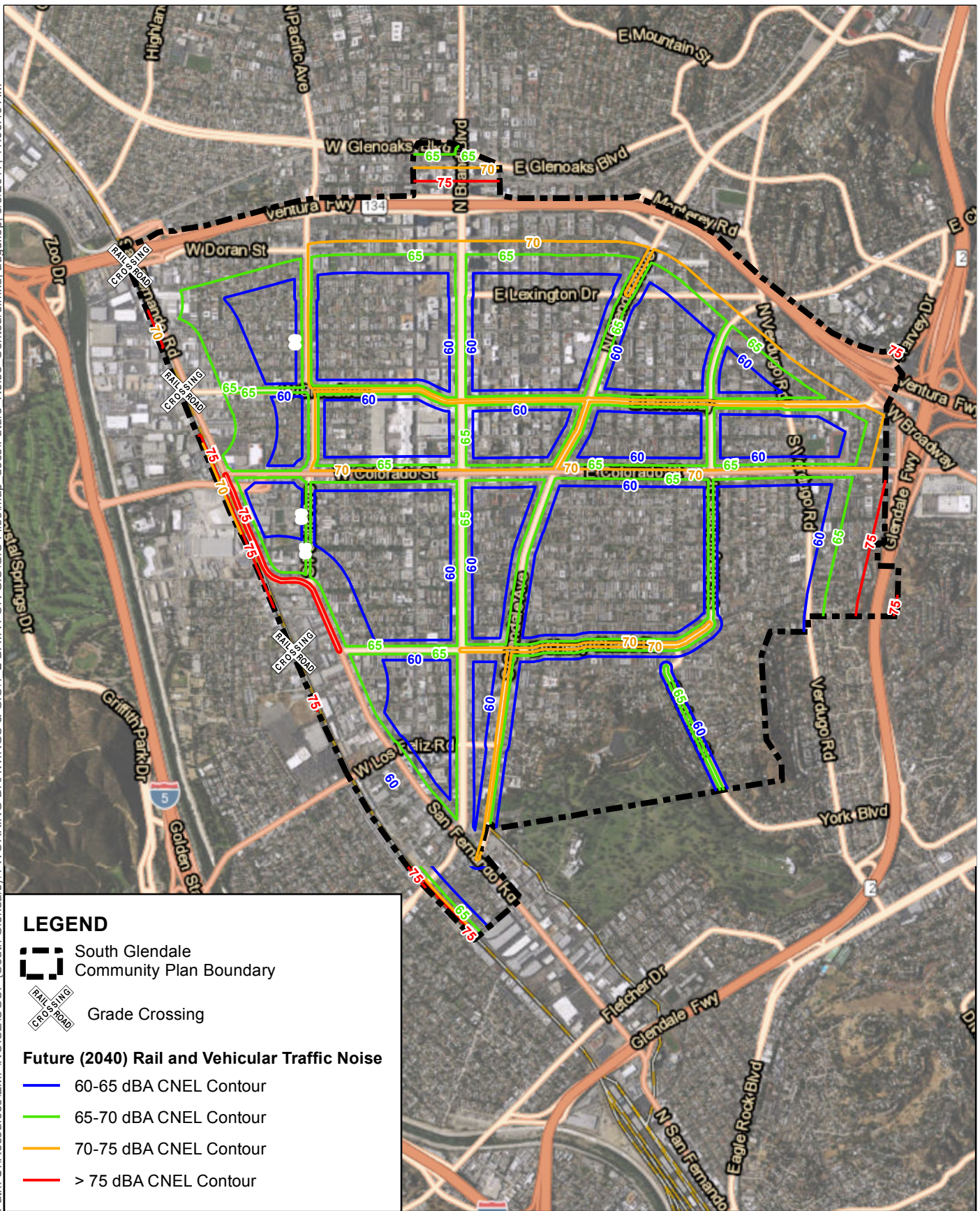


Source: Esri, HERE, DeLorme, © OpenStreetMap contributors; DigitalGlobe, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, IGN, and the GIS User Community

FIGURE 6.1-1
EXISTING (2017) RAIL AND VEHICULAR
TRAFFIC NOISE CONTOURS
 SOUTH GLENDALE COMMUNITY PLAN



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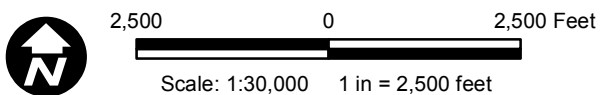
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- South Glendale Community Plan Boundary
- Grade Crossing

Future (2040) Rail and Vehicular Traffic Noise

- 60-65 dBA CNEL Contour
- 65-70 dBA CNEL Contour
- 70-75 dBA CNEL Contour
- > 75 dBA CNEL Contour

Source: Esri, HERE, DeLorme, © OpenStreetMap contributors; DigitalGlobe, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, IGN, and the GIS User Community



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FIGURE 6.1-2
FUTURE (2040) RAIL AND VEHICULAR
TRAFFIC NOISE CONTOURS
SOUTH GLENDALE COMMUNITY PLAN

6.1.2 Rail Noise

Railway noise is generated from the rail traffic along the SGCP area western boundary, consisting of freight trains and passenger rail (Amtrak and Metrolink). The corridor contains a total of three at-grade crossings located at Chevy Chase Drive, Broadway, and Doran Street. Predicted noise levels in proximity to these grade crossings assumed the occurrence of train horn soundings as outlined in Section 5.1.2. Additionally, modeled passenger train speeds were reduced to 15 mph in the vicinity of the Larry Zarian Transportation Center to reflect the slowing and stopping of passenger trains at the station.

Prediction model results shown in Table 6.1-2 provide 60 dBA L_{dn} noise contour distances that are calculated assuming flat-site conditions and no intervening existing buildings or barriers that would provide noise attenuation, which would represent a conservative, worst-case analysis.

Detailed FTA model runs showing modeled input parameters and detailed results are included in Attachment B.

Source	Rail Section Scenario		
	Typical, No Slowing, No Horn Sounding	Transit Center Vicinity, With Slowing, No Horn Sounding	Grade Crossing, No Slowing, With Horn Sounding
Metrolink Passenger Rail	120 feet	190 feet	880 feet
Amtrak Passenger Rail	30 feet	47 feet	218 feet
Freight Rail	87 feet	87 feet	280 feet
Aggregate of Rail Sources	180 feet	245 feet	1060 feet

The California High-Speed Rail Authority is currently studying use of the current railroad right-of-way on the western border of the SGCP area as a portion of the planned Burbank to Los Angeles Project Section of their planned California High Speed Rail service, although final designs and the date that service will begin are still under development. The section that borders the SGCP (along the existing rail corridor), if it is built, would be constructed either at-grade or on an elevated viaduct to avoid existing grade-crossings, and eliminating horn sounding requirements. The combined acoustical effect of higher train speeds and number of trains (which would increase rail noise exposure), the elimination of required train horn sounding at grade crossing for all train types (which would lower rail noise exposure), and ultimate changes in the vertical and horizontal alignment of the future rail lines in this area (acoustical effect unknown), are not known at this time. However, the elimination of horn sounding at the three grade crossings adjacent to the SGCP area, would, by itself, result in a substantial noise reduction in the areas within several hundred feet of the grade crossings. It is assumed that future operation of the Burbank to Los Angeles Project Section would implement appropriate mitigation measures to avoid noise-related impacts, and thus, is not expected to extend future CNEL contributions from the railroad right-of-way. However, the increase in quantity in existing rail services along the railroad right-of-way may have a much greater influence on future CNEL levels.

As reported in the Technical Appendix to the City of Glendale Noise Element of the General Plan (Mestre Greve Associates 2005), Metrolink representatives were noted stating that train operations by the year 2030 will increase to ninety-six (96) trains per day, a growth in trip quantity of approximate 34%. It was also assumed within the same document that freight rail usage would increase by 33% from ten (10) trains per day to fifteen (15) trains per day. The document also stated that Amtrak did not imply that any plans were made for changes in its service through the corridor. As shown in Table 6.1-3, the aggregate operation of future rail uses extend the 60 dBA L_{dn} a notable distance into the SGCP area.

Table 6.1 3
Distance of Predicted Future 60 dBA (L_{dn}) Noise Levels from Rail Center Alignment

Source	Rail Section Scenario		
	Typical, No Slowing, No Horn Sounding	Transit Center Vicinity, With Slowing, No Horn Sounding	Grade Crossing, No Slowing, With Horn Sounding
Metrolink Passenger Rail	160 feet	254 feet	1170 feet
Amtrak Passenger Rail	30 feet	47 feet	218 feet
Freight Rail	128 feet	113 feet	370 feet
Aggregate of Rail Sources	235 feet	320 feet	1460 feet

The railroad corridor is lined with varying land use types, primarily comprised of commercial retail, storage warehouses and yards, and parking lots. One segment of railway abuts the residential neighborhood of single family and multi-family homes between Glendale Boulevard and Tyburn Street. Similar to vehicular noise levels generated by vehicular traffic noise, future rail operation noise levels within the proposed SGCP area at existing and proposed residential use areas would, in cases of proposed single-family and multi-family residences close to the rail alignment, exceed the General Plan Noise Element thresholds and standards.

6.1.3 Municipal Code Compliance

Proposed mixed-use areas would contain residential, commercial, and industrially permitted developments. Where residential uses are located in proximity to commercial or industrial sites, noise sensitive receptors are likely to be exposed to additional noise aside from traffic noise contributions found throughout the SGCP area. These noise sensitive receptors could be exposed to noise due to operations traffic, truck idling, loading and unloading operations, mechanical equipment such as HVAC units and air handlers, trash-hauling activities, and customer/employee use of commercial facilities.

While noise-sensitive residential land uses would be exposed to noise associated with the operation of commercial uses, policies are in place to control noise and reduce noise impacts between various land uses. Noise policies, as contained in the General Plan Noise Element, the proposed SGCP, and regulations in the GMC are in place to control and reduce noise levels from various land uses to levels below impact thresholds by zone. These include the requirement for noise studies for certain new developments, limits on hours of operation for various noise-generating activities, and standards for the compatibility of land use types. In addition, enforcement of the federal, state, and local noise regulations would control impacts. Given implementation of these policies and enforcement of the Noise Control chapter of the GMC, impacts would be less than significant.

6.2 Exposure of persons to or generation of excessive groundborne vibration or groundborne noise levels

6.2.1 Commercial Uses

Commercial and industrial operations often utilize equipment or conduct processes which may generate vibration to land uses in close proximity to the source. Vibrations generated by such operations are generally regulated from an occupational health and safety perspective, the effect of which would reduce the exposure of employees to excessive vibration and as a result, also reduce the exposure of abutting land uses. Vibrations from operations typically of low amplitude and attenuate sharply as they traverse through the surrounding soil. The proposed land uses within the SGCP and associated discretionary actions includes retail facilities, restaurants, and office spaces that would not require heavy mechanical equipment or heavy truck deliveries, both of which could generate atypical levels of vibration. Additional proposed land uses, such as residential developments and civic uses do not typically generate any notable vibration. Thus, operational vibration impacts associated with the implementation of the proposed SGCP and associated discretionary actions implementation would be less than significant.

6.2.2 Construction Activities

Construction activities can generate groundborne vibration of varying degrees based on the construction activity and equipment being used. Groundborne vibration and noise associated with construction activities would only occur temporarily during groundbreaking activities such as demolition, pile driving or caisson drilling, and excavation for underground levels, and vibratory pile driving could be used to stabilize the walls of excavated areas. However, non-pile driving or foundation work construction phases that have the highest potential of producing vibration would be intermittent and only occur for short periods of time. The Caltrans Transportation and Construction Vibration Guidance Manual (Caltrans 2013) identifies potential vibration damage thresholds for various structure types and human receptors as measured by PPV, in inches per second. By use of administrative controls, such as scheduling vibration-intensive construction activities to hours with the least potential to affect nearby sensitive receptors, perceptible vibration can be kept to a minimum and, as such, would result in a less than significant impact.

Pile driving has the potential to generate the highest groundborne vibration levels and is the primary concern human perception. As discussed in Section 3.1.3, pile driving or other intermittent or continuous vibratory construction can result in distinct human perception at a vibratory level of .04 PPV in/sec. human receptors experience “strongly perceptible” vibration at 0.1 PPV in/sec. The construction of future land uses as a result of the implementation of the proposed SGCP and associated discretionary actions would have the potential to result in a significant impact related to vibration associated with construction.

6.3 A substantial permanent increase in ambient noise levels in the project vicinity above levels existing without the project

Existing stationary noise sources identified within the community plan area were typical of a developed mixed-use neighborhood, including HVAC units in operation and noise associated with commercial uses such as automotive mechanic shops. Although the SGCP proposes the development of land uses which may ultimately generate noise during operations, operational noise levels would be required to comply with the GMC and General Plan guidelines.

Noise from vehicular traffic is the prominent source of noise in the SGCP area and has greater potential to affect existing noise-sensitive receivers if annual average daily traffic volumes increase substantially. The freeways generating the greatest noise levels affecting the SGCP area are SR-2 and SR-134. The streets generating the greatest noise levels within the area are Chevy Chase Drive, Colorado Avenue, and Glendale Avenue. Vehicular traffic volumes on roadways in the community plan area would generally increase due to the future development proposed by the SGCP and associated discretionary actions, however, some roadway volumes will decrease. Table 6.1-4 summarizes the existing and future traffic noise levels along various roadway segments in the SGCP area. Roadway noise is reported in this table as the dBA CNEL at 50 feet from the roadway EOP.

Roadway	Roadway Segment	Predicted Ambient Noise Level (dBA, CNEL @ 50 Feet from EOP)		
		Existing (2017)	Future (2040)	Change in dB
Brand Boulevard	North of Lexington Drive	65	65	0
	North of Broadway	64	65	1
	North of Colorado St	65	65	0
	North of Chevy Chase Drive	63	64	1
	North of Los Feliz Road	64	65	1
	North of San Fernando Road	64	65	1
Broadway	East of San Fernando Road	61	63	1
	East of Pacific Avenue	64	65	1
	East of Brand Boulevard	65	65	0
	East of Glendale Avenue	65	66	1

Table 6.1 4 Increases in Ambient Noise for the South Glendale Community Plan Area				
Roadway	Roadway Segment	Predicted Ambient Noise Level (dBA, CNEL @ 50 Feet from EOP)		
		Existing (2017)	Future (2040)	Change in dB
	East of Verdugo Road	67	67	0
Chevy Chase Drive	East of San Fernando Road	65	65	0
	East of Brand Boulevard	66	67	2
	East of Glendale Avenue	66	67	0
	North of Acacia Avenue	64	62	-2
	North of Colorado St	66	64	-1
	North of Broadway	64	64	0
Colorado Street	East of San Fernando Road	63	64	1
	East of Pacific Avenue	68	68	1
	East of Brand Boulevard	67	68	1
	East of Glendale Avenue	67	68	1
	East of Verdugo Road	67	68	1
Glendale Avenue	North of Lexington Drive	67	67	-1
	North of Broadway	65	66	0
	North of Colorado St	65	66	1
	North of Chevy Chase Drive	64	65	1
	North of Los Feliz Road	65	66	1
	North of San Fernando Road	64	65	2
Pacific Avenue	North of Lexington Drive	66	66	0
	North of Broadway	65	66	0
	North of Colorado St	65	66	0
	North of San Fernando Road	62	62	0
	North of Broadway	66	67	1
San Fernando Road	North of Colorado St	66	67	1
	North of Chevy Chase Drive	69	70	1
	North of Los Feliz Road	67	68	1
	East of Brand Boulevard	68	69	1
	East of Verdugo Road	62	62	0
York Boulevard / South Adams Street	North of Lexington Drive	65	65	0
Freeways				

**Table 6.1 4
Increases in Ambient Noise for the South Glendale Community Plan Area**

Roadway	Roadway Segment	Predicted Ambient Noise Level (dBA, CNEL @ 50 Feet from EOP)		
		Existing (2017)	Future (2040)	Change in dB
State Route 134	At Pacific Avenue	83	83	0
	At Central Avenue / Brand Boulevard	83	83	0
	At Glendale Avenue	83	83	0
State Route 2	At York Boulevard / Delevan Street	81	81	0

CNEL = Community Noise Equivalent Level; dBA = A-weighted decibel; EOP = edge of pavement
Bold = 2040 noise level would exceed the established exterior compatibility level for the surrounding land use and noise levels would increase by 3 dB or more, or future noise levels would be below 65 dBA CNEL but ambient noise levels would increase by more than 5 dBA over existing noise levels.

As shown in Table 6.1-4, no roadway segments that are generating existing noise levels greater than 65 dBA CNEL are predicted to generate an increase in noise levels greater than 2 dBA in the future condition. Additionally, no roadway segments currently generate noise levels lower than 65 dBA CNEL that are predicted to increase in by more than 5 dBA over existing ambient noise levels, thus, ambient noise level increases at existing noise sensitive land uses would be less than significant.

6.4 A substantial temporary or periodic increase in ambient noise levels in the project vicinity above levels existing without the project

6.4.1 Construction Noise

Although no specific construction or development is proposed under the proposed SGCP and associated discretionary actions at this time, construction noise could occur as future development occurs. Due to the highly-developed nature of land uses within SGCP area, there is a high likelihood that construction activities would take place adjacent to noise sensitive land uses.

It is assumed that any future construction projects within the SGCP and in proximity to noise sensitive area (especially single and multi-family residential land uses) related to the SGCP or not, would be required to conduct separate environmental review to ensure that the project is in compliance with the City of Glendale Municipal Code, particularly Section 8.36.080 for construction noise and apply any required noise mitigation elements. Mitigation requirement would be project specific, but could include such measures as temporary noise wall or curtains, use of quieter equipment and construction procedures, and restrictions on nighttime construction.

6.5 Projects located within an airport land use plan

The nearest public or private airport, Hollywood Burbank Airport, is located approximately 5.1 miles northwest of the study area. The Los Angeles County Airport Land Use Plan (Los Angeles 1991) does not include the SGCP area within any airport's Planning Boundary/Airport Influence Area. While aircraft overflights may sometime be audible in the SGCP area these would not be considered a dominant noise source and would have little impact on existing or future CNEL noise levels.

6.6 Project within the vicinity of a private airstrip

No private airstrips are known to exist within several miles of the SGCP, so this will not create any impacts.

7. Summary of Predicted Impacts and Mitigation

The following is a summary of impacts for each significance threshold addressed in Section 7. For significant impacts, program-level mitigation is identified where feasible, and the subsequent mitigation framework identifies measures to be applied to future development projects within the SGCP area to reduce noise impacts when and where they occur.

7.1 Increase in Ambient Noise Levels

As indicated in Table 6.1-4, increases in ambient noise for the SGCP area as a result of increases in surface transportation is expected to range from -2 to + 2 dBA CNEL, which would be expected to be less than noticeable, and less than significant, so no specific SGCP-wide impacts are expected nor is mitigation required associated with increases in ambient noise levels.

7.2 Exposure to Existing and Future Transportation Noise

7.2.1 Vehicle Traffic Noise Exposure

While SGCP-related increases in traffic are not expected to result in significant noise increases, there may be areas where noise sensitive land uses are already in excess of local guidelines for existing conditions, such as the Land Use Noise Compatibility Guidelines from the City's General Plan Noise Element, presented in Table 3.1-2 of this report. This may be especially true for residential properties along busy arterial corridors and control access highways. However, since this represents no significant change from the existing condition, noise mitigation would not be required for existing developments.

7.2.2 Rail Noise Exposure

Similar to vehicle traffic noise exposure, noise exposure from rail activity on the existing rail line would not see a significant increase (2 dBA or less); but, some areas near the rail line, and especially near the grade crossings at Chevy Chase, West Broadway, and Doran, are already above Noise Compatibility Guidelines. However, since this is an existing condition with no significant increase, no noise mitigation would be required at this time.

Extra attention should be paid to the on-going future development of the rail line for the planned California High Speed Rail Project which is expected to share the rail corridor bordering the SGCP area in the future. The design plans and timing for high speed rail in this area are still under development, but the future implementation of the project (if and when it actually goes into operation) may have an impact on noise levels in the SGCP. At the least, it is expected that the at-grade crossings will be replaced with grade separations for both new and existing rail traffic, eliminating the need for horn soundings, and thereby reducing horn noise. It is also possible that other rail noise mitigation elements such as noise walls may also be installed as part of that project.

7.3 General Plan Compliance

As noted above, noise levels for existing conditions, dominated by surface transportation sources, may already exceed land use compatibility guidelines at several existing noise sensitive developments in the SGCP, particularly near arterial and controlled access roadways and near rail lines. Generally, it would not be required to provide noise mitigation to areas impacted under existing conditions. However, any new development of noise sensitive land uses within the SGCP area (whether associated with SGCP projects or not) would likely require a detailed noise analysis as part of the planning stage, complete with recommended noise mitigation measures to insure compliance with guidelines. The recommended mitigation elements, if required, would be project-specific but could include the some or all of the following:

- Increase setback of dwelling units from area roadways or rail lines.
- Use of developer-installed noise walls to protect exterior use areas.
- Use of upgraded acoustical doors and windows dwelling units to reduce interior noise.
- Use of air conditioning or ventilation systems to enable windows to remain closed.
- Use of parking areas or garage structures to act as acoustical buffers or barriers against highway or rail noise.

It is expected that the acoustical analysis would be conducted by an experienced acoustical engineer as part of the project approval process, should a study be deemed necessary during the environmental review process associated with future development projects.

7.4 Municipal Code Compliance

The municipal code for noise and vibration is addressed under Municipal Code Chapter 8.36 Noise Control and described in detail in Section 3.1.4 of this report. This would apply primarily to temporary noise and vibration from construction activities as well as on-going building operations, such as building air conditioning/ventilation systems and any other noise producing elements. Normally the analysis and required mitigation of construction and building noise would be determined as part of a required project-specific noise analysis.

7.4.1 Construction and Vibration

Construction noise is address under Code section 8.36.0808 and primarily prohibits construction activity within 500 feet of a residential zone during nighttime periods, weekends and certain holidays. Therefore, the primary mitigation element would be to avoid construction activity during those periods.

Code Section 8.36.210 addresses vibration, stating that any vibration level should not exceed the vibration perception threshold beyond the property line. Perceptible vibration would normally only be expected under certain construction processes, such as pile driving and some demolition activities. Possible mitigation elements would include using alternative pile driving processes, such as vibratory or pre-augured pile. In some cases of particularly sensitive neighbors, vibration sensitive land uses, or older fragile buildings, vibration monitoring may also be required.

7.4.2 Operation

Noise from regular building operations would be regulated by the noise level standards in Code Section 8.36.040, including 45 dBA nighttime and 55 dBA daytime limits in a residential zone, and would primarily be analyzed for building HVAC, but could also include sounds from other exposed or externally vented equipment, transformers, pool pumps and filtration equipment, outdoor entertainment systems or any other noise producing equipment or activities. If these levels attributed to proposed project building operations were determined to exceed applicable thresholds, noise mitigation options could include some or all of the following:

- Specify quieter equipment.
- Use acoustical panels or enclosures around exposed noise producing equipment.
- Relocate noise-producing equipment into an acoustically-isolated space.
- Relocate noise-producing equipment to be further from noise-sensitive property boundaries.
- Apply appropriate silencers, mufflers, baffles or other noise reducing modifications to noisy equipment.

8. References

California Department of Transportation (Caltrans)

- 2011 Traffic Noise Analysis Protocol for New Highway Construction, Reconstruction, and Retrofit Barrier Projects, California Department of Transportation, May 2011.
- 2013 Transportation and Construction Vibration Guidance Manual. Division of Environmental Analysis. September 2013.

California High Speed Rail Authority (CHRA)

- 2017 Burbank to Los Angeles Section, June 2017 Update: http://www.hsr.ca.gov/Programs/Statewide_Rail_Modernization/Project_Sections/burbank_losangeles_update_june_2017.html.

City of Glendale

- 2007 City of Glendale General Plan Noise Element, May 2007.
- 1991 City of Glendale Municipal Code, Chapter 8.36 Noise Control.

Federal Transit Administration (FTA)

- 2006 Transit Noise and Vibration Impact Assessment FTA-VA-90-1003-06. Office of Planning and Environment. May 2006.

Fehr & Peers

- 2017 South Glendale Community Plan Draft Transportation Analysis Report, July 2017.

Attachment A – Field Measurement Data

Measurement ID	Date	Time	Duration (hh:mm)	LA _{eq}	L _{min}	L _{max}	L ₁₀	L ₅₀	L ₉₀
ST-1	2017-07-18	09:23:00	00:01	50.4	46.1	55.1	52.6	50.1	46.6
	2017-07-18	09:24:00	00:01	51.0	45.5	58.8	55.2	47.4	45.8
	2017-07-18	09:25:00	00:01	48.8	45.3	59.2	51.3	46.6	45.6
	2017-07-18	09:26:00	00:01	49.8	45.3	56.7	53.1	46.3	45.5
	2017-07-18	09:27:00	00:01	56.7	49.3	68.0	60.2	52.8	50.4
	2017-07-18	09:28:00	00:01	68.3	55.9	75.8	73.4	63.7	57.2
	2017-07-18	09:29:00	00:01	68.7	53.2	78.3	74.6	58.2	53.7
	2017-07-18	09:30:00	00:01	59.5	53.6	67.4	64.4	56.7	54.5
	2017-07-18	09:31:00	00:01	53.8	53.0	54.5	54.2	53.8	53.2
	2017-07-18	09:32:00	00:01	56.1	53.5	59.0	58.3	55.2	54.2
	2017-07-18	09:33:00	00:01	53.6	51.6	56.0	55.1	53.9	52.0
	2017-07-18	09:34:00	00:01	52.7	51.8	54.3	53.3	52.6	52.1
	2017-07-18	09:35:00	00:01	52.9	52.1	54.2	53.6	52.8	52.4
	2017-07-18	09:36:00	00:01	53.3	52.2	56.5	53.8	53.0	52.5
2017-07-18	09:37:00	00:01	53.2	52.2	56.3	53.8	53.1	52.6	
ST-2	2017-07-18	10:09:00	00:01	60.3	51.9	67.3	63.5	59.4	52.5
	2017-07-18	10:10:00	00:01	56.2	51.1	63.1	57.8	55.6	52.1
	2017-07-18	10:11:00	00:01	58.7	53.5	64.8	62.9	56.5	54.3
	2017-07-18	10:12:00	00:01	60.0	52.5	72.8	59.1	56.1	53.5
	2017-07-18	10:13:00	00:01	58.2	51.2	67.4	60.7	55.2	51.8
	2017-07-18	10:14:00	00:01	56.2	51.8	61.1	59.2	55.4	53.3
	2017-07-18	10:15:00	00:01	55.0	50.3	58.6	57.5	54.3	50.6
	2017-07-18	10:16:00	00:01	56.6	50.0	62.2	60.3	55.0	51.3
	2017-07-18	10:17:00	00:01	57.4	52.2	65.7	59.2	55.1	54.0
	2017-07-18	10:18:00	00:01	57.9	54.0	64.8	60.0	57.0	54.3
	2017-07-18	10:19:00	00:01	54.3	51.1	57.9	56.6	53.7	51.5
	2017-07-18	10:20:00	00:01	56.6	51.5	63.0	59.5	55.3	52.1
	2017-07-18	10:21:00	00:01	57.4	52.6	61.3	59.3	57.4	53.5
	2017-07-18	10:22:00	00:01	54.8	52.2	58.9	57.3	54.0	52.5
2017-07-18	10:23:00	00:01	57.3	52.0	60.2	59.7	57.5	53.2	
ST-3	2017-07-18	10:41:00	00:01	70.1	58.3	75.7	74.0	67.6	60.7
	2017-07-18	10:42:00	00:01	71.4	57.5	76.5	74.7	71.3	59.6
	2017-07-18	10:43:00	00:01	70.5	55.2	75.2	73.5	70.2	59.1
	2017-07-18	10:44:00	00:01	68.4	55.2	74.9	72.2	67.1	56.6
	2017-07-18	10:45:00	00:01	70.7	59.9	75.8	73.8	69.6	65.1
	2017-07-18	10:46:00	00:01	69.0	60.5	77.5	72.2	67.2	62.1
	2017-07-18	10:47:00	00:01	71.7	65.6	75.9	74.7	70.5	67.2
	2017-07-18	10:48:00	00:01	68.7	55.2	76.6	72.8	66.6	56.6
	2017-07-18	10:49:00	00:01	70.8	54.8	77.1	74.7	69.4	55.8
	2017-07-18	10:50:00	00:01	69.9	60.4	75.9	74.2	68.4	62.4
	2017-07-18	10:51:00	00:01	69.7	53.9	74.8	72.8	69.5	57.0
	2017-07-18	10:52:00	00:01	70.7	57.5	76.2	74.2	69.6	61.8
	2017-07-18	10:53:00	00:01	67.7	53.0	72.7	71.4	67.4	55.3
	2017-07-18	10:54:00	00:01	68.6	57.6	74.3	70.9	68.4	62.9
2017-07-18	10:55:00	00:01	72.8	57.7	82.3	75.9	69.3	61.1	
ST-4	2017-07-18	11:11:00	00:01	63.0	61.3	64.5	63.8	62.9	62.1
	2017-07-18	11:12:00	00:01	64.6	61.5	67.1	66.3	64.3	62.2
	2017-07-18	11:13:00	00:01	69.0	62.5	77.1	74.3	65.3	63.1
	2017-07-18	11:14:00	00:01	62.9	60.7	65.5	64.7	62.4	61.5
	2017-07-18	11:15:00	00:01	62.7	60.6	66.1	65.1	61.9	61.2
	2017-07-18	11:16:00	00:01	62.6	60.2	65.0	64.0	62.3	60.8
	2017-07-18	11:17:00	00:01	62.8	60.4	65.2	64.1	62.5	60.8
	2017-07-18	11:18:00	00:01	64.6	60.8	68.0	67.1	63.9	61.9
	2017-07-18	11:19:00	00:01	63.1	60.8	65.2	64.4	63.2	61.3
	2017-07-18	11:20:00	00:01	64.5	61.0	71.7	68.2	62.7	61.6
	2017-07-18	11:21:00	00:01	65.8	61.0	72.6	68.8	64.1	62.4
	2017-07-18	11:22:00	00:01	63.6	61.4	66.4	64.8	63.4	61.7
	2017-07-18	11:23:00	00:01	66.2	62.7	74.6	66.0	64.0	63.3
	2017-07-18	11:24:00	00:01	65.4	61.9	72.1	69.7	64.0	62.5
2017-07-18	11:25:00	00:01	63.2	61.5	65.4	64.7	63.0	62.3	

Measurement ID	Date	Time	Duration (hh:mm)	LA _{eq}	L _{min}	L _{max}	L ₁₀	L ₅₀	L ₉₀
ST-5	2017-07-18	12:04:00	00:01	58.8	51.5	64.4	62.1	57.6	52.0
	2017-07-18	12:05:00	00:01	57.5	53.3	62.2	59.6	57.2	54.2
	2017-07-18	12:06:00	00:01	60.2	53.0	73.7	59.4	57.9	55.1
	2017-07-18	12:07:00	00:01	57.6	53.3	61.8	60.3	57.0	54.6
	2017-07-18	12:08:00	00:01	57.6	51.6	61.9	61.0	56.4	52.7
	2017-07-18	12:09:00	00:01	57.5	52.6	62.6	60.2	56.6	54.1
	2017-07-18	12:10:00	00:01	57.8	51.7	63.8	61.1	56.7	52.9
	2017-07-18	12:11:00	00:01	57.1	50.6	61.5	59.6	57.2	51.9
	2017-07-18	12:12:00	00:01	56.6	50.5	68.0	58.7	54.9	52.3
	2017-07-18	12:13:00	00:01	60.5	55.8	67.8	62.2	60.1	56.7
	2017-07-18	12:14:00	00:01	60.8	58.2	65.0	62.4	60.3	59.3
	2017-07-18	12:15:00	00:01	61.7	57.9	66.0	63.6	61.0	58.6
	2017-07-18	12:16:00	00:01	60.6	55.8	66.2	63.1	59.6	57.7
	2017-07-18	12:17:00	00:01	61.1	54.5	67.7	64.2	60.5	55.0
2017-07-18	12:18:00	00:01	60.1	54.9	65.5	61.7	60.0	55.3	
ST-6	2017-07-18	15:17:00	00:01	64.6	57.5	70.0	67.9	63.5	59.2
	2017-07-18	15:18:00	00:01	60.0	55.6	64.0	62.2	59.6	56.5
	2017-07-18	15:19:00	00:01	59.8	54.9	65.9	62.7	59.1	55.8
	2017-07-18	15:20:00	00:01	62.4	54.2	68.4	66.6	58.0	55.3
	2017-07-18	15:21:00	00:01	63.6	55.4	72.5	66.9	61.8	56.9
	2017-07-18	15:22:00	00:01	75.9	55.4	88.2	77.8	61.2	56.4
	2017-07-18	15:23:00	00:01	65.9	56.0	75.2	70.4	61.0	58.5
	2017-07-18	15:24:00	00:01	60.6	54.6	66.2	64.0	59.7	55.9
	2017-07-18	15:25:00	00:01	61.4	55.2	67.9	65.6	58.8	55.9
	2017-07-18	15:26:00	00:01	61.9	55.3	68.0	64.8	61.3	56.9
	2017-07-18	15:27:00	00:01	62.1	55.4	68.0	64.9	61.3	57.4
	2017-07-18	15:28:00	00:01	59.5	54.1	66.3	62.3	57.9	55.2
	2017-07-18	15:29:00	00:01	62.1	55.6	68.6	65.7	61.1	56.6
	2017-07-18	15:30:00	00:01	61.8	57.4	65.8	63.9	60.8	58.3
2017-07-18	15:31:00	00:01	64.9	56.1	74.5	69.4	60.1	58.0	
ST-7	2017-07-18	14:44:00	00:01	59.7	57.7	62.1	61.3	59.1	58.4
	2017-07-18	14:45:00	00:01	60.4	58.0	67.4	62.1	59.5	58.4
	2017-07-18	14:46:00	00:01	59.6	57.7	61.8	60.8	59.3	58.2
	2017-07-18	14:47:00	00:01	58.9	56.9	62.2	60.2	58.8	57.2
	2017-07-18	14:48:00	00:01	59.7	57.8	68.9	60.3	58.7	58.1
	2017-07-18	14:49:00	00:01	62.9	57.0	74.0	65.2	58.5	57.7
	2017-07-18	14:50:00	00:01	60.3	57.6	67.0	62.6	59.2	58.1
	2017-07-18	14:51:00	00:01	58.2	55.0	60.5	59.6	58.3	56.2
	2017-07-18	14:52:00	00:01	58.7	55.4	63.4	60.6	58.5	56.0
	2017-07-18	14:53:00	00:01	62.0	55.6	73.5	60.9	58.4	56.5
	2017-07-18	14:54:00	00:01	56.9	55.5	70.5	58.0	56.6	55.9
	2017-07-18	14:55:00	00:01	60.9	55.4	70.0	64.9	57.8	55.9
	2017-07-18	14:56:00	00:01	60.8	58.6	65.2	61.8	60.1	59.4
	2017-07-18	14:57:00	00:01	59.1	55.6	62.2	60.7	58.9	56.1
2017-07-18	14:58:00	00:01	58.9	56.9	66.5	59.7	58.2	57.2	
ST-8	2017-07-18	14:16:00	00:01	62.0	51.9	69.3	67.0	55.6	52.7
	2017-07-18	14:17:00	00:01	53.7	48.9	63.0	55.0	51.5	49.8
	2017-07-18	14:18:00	00:01	51.5	48.2	59.2	54.0	50.1	48.8
	2017-07-18	14:19:00	00:01	53.3	48.5	61.3	55.6	51.5	50.0
	2017-07-18	14:20:00	00:01	51.6	47.6	59.2	54.1	49.6	48.9
	2017-07-18	14:21:00	00:01	54.8	48.3	63.1	60.7	50.4	49.1
	2017-07-18	14:22:00	00:01	51.3	47.2	58.3	53.9	48.7	47.6
	2017-07-18	14:23:00	00:01	48.1	46.9	50.8	48.7	47.9	47.5
	2017-07-18	14:24:00	00:01	55.4	48.2	61.3	59.5	51.7	48.5
	2017-07-18	14:25:00	00:01	52.5	48.1	60.0	57.0	50.2	48.5
	2017-07-18	14:26:00	00:01	54.2	47.2	60.4	57.6	52.3	48.3
	2017-07-18	14:27:00	00:01	51.5	47.7	60.1	53.1	49.5	48.0
	2017-07-18	14:28:00	00:01	50.7	47.6	57.6	52.5	49.4	48.1
	2017-07-18	14:29:00	00:01	53.9	47.6	62.2	56.3	51.2	48.4
2017-07-18	14:30:00	00:01	55.2	52.2	61.8	57.3	54.1	52.6	

Attachment B – Rail Operations Input Data and FTA Calculation

Timetable Breakdown - Quantity Per Period (Existing Condition)

Operator / Line	Day	Evening	Night
Metrolink Ventura County	27	2	4
Metrolink Antelope Valley	24	3	3
Amtrak Pacific Surfliner	8	2	0
Amtrak Starlight	1	1	0
Freight (GP Appendix - "10")	8	1	1

Existing - by Rail Service

Scenario	Service	Loco	Day Hourly	Night Hourly	Speed
Typical , No Horn, No Slowing	Metrolink	1	4.67	0.58	30
	Amtrak	1	1.00	0.00	30
	Freight	3	0.75	0.08	30
	Freight - Rail Car	80 Cars	0.75	0.08	30
Transit Center , No Horn, With Slowing	Metrolink	1	4.67	0.58	15
	Amtrak	1	1.00	0.00	15
	Freight	3	0.75	0.08	30
	Freight - Rail Car	80 Cars	0.75	0.08	30
Grade Crossing , With Horn, No Slowing	Metrolink	1	4.67	0.58	30
	Metrolink Horn	-	2.34	0.29	30
	Amtrak	1	1.00	0.00	30
	Amtrak Horn	-	0.50	0.00	30
	Freight	3	0.75	0.08	30
	Freight - Rail Car	80 Cars	0.75	0.08	30
	Freight Horn	-	0.38	0.04	30

Future - by Rail Service

Scenario	Service	Loco	Day Hourly	Night Hourly	Speed
Typical , No Horn, No Slowing	Metrolink	1	7.11	0.89	30
	Amtrak	1	1.00	0.00	30
	Freight	3	1.13	0.13	30
	Freight - Rail Car	80 Cars	1.13	0.13	30
Transit Center , No Horn, With Slowing	Metrolink	1	7.11	0.89	15
	Amtrak	1	1.00	0.00	15
	Freight	3	1.13	0.13	30
	Freight - Rail Car	80 Cars	1.13	0.13	30
Grade Crossing , With Horn, No Slowing	Metrolink	1	7.11	0.89	30
	Metrolink Horn	-	3.56	0.45	30
	Amtrak	1	1.00	0.00	30
	Amtrak Horn	-	0.50	0.00	30
	Freight	3	1.13	0.13	30
	Freight - Rail Car	80 Cars	1.13	0.13	30
	Freight Horn	-	0.56	0.06	30

Existing - Aggregate

Scenario	Service	Loco	Day Hourly	Night Hourly	Speed
Typical , No Horn, No Slowing	Passenger	1	5.67	0.58	30
	Freight	3	0.75	0.08	30
	Freight - Rail Car	80 Cars	0.75	0.08	30
Transit Center , No Horn, With Slowing	Passenger	1	5.67	0.58	15
	Freight	3	0.75	0.08	30
	Freight - Rail Car	80 Cars	0.75	0.08	30
Grade Crossing , With Horn, No Slowing	Passenger	1	4.67	0.58	30
	Freight	3	0.75	0.08	30
	Freight - Rail Car	80 Cars	0.75	0.08	30
	Horn	-	3.09	0.37	30

Future - Aggregate

Scenario	Service	Loco	Day Hourly	Night Hourly	Speed
Typical , No Horn, No Slowing	Passenger	1	8.11	0.89	30
	Freight	3	1.13	0.13	30
	Freight - Rail Car	80 Cars	1.13	0.13	30
Transit Center , No Horn, With Slowing	Passenger	1	8.11	0.89	15
	Freight	3	1.13	0.13	30
	Freight - Rail Car	80 Cars	1.13	0.13	30
Grade Crossing , With Horn, No Slowing	Passenger	1	8.11	0.89	30
	Freight	3	1.13	0.13	30
	Freight - Rail Car	80 Cars	1.13	0.13	30
	Horn	-	5.18	0.57	30

Project:	South Glendale CP
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Noise Source Parameters	Number of Noise Sources: 3
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Noise Source Parameters		Source 1
	Source Type:	Fixed Guideway
	Specific Source:	Diesel Electric Locomotive
Daytime hrs	Avg. Number of Locos/train	1
	Speed (mph)	30
	Avg. Number of Events/hr	5.67
Nighttime hrs	Avg. Number of Locos/train	1
	Speed (mph)	30
	Avg. Number of Events/hr	0.58
Distance	Distance from Source to Receiver (ft)	180
	Number of Intervening Rows of Buildings	0
Adjustments		No
		No
		No
		No

Source 1 Results

Leq(day):	57.8 dBA
Leq(night):	47.9 dBA
Ldn:	57.8 dBA

Noise Source Parameters		Source 2
	Source Type:	Fixed Guideway
	Specific Source:	Diesel Electric Locomotive
Daytime hrs	Avg. Number of Locos/train	3
	Speed (mph)	30
	Avg. Number of Events/hr	0.75
Nighttime hrs	Avg. Number of Locos/train	3
	Speed (mph)	30
	Avg. Number of Events/hr	0.08
Distance	Distance from Source to Receiver (ft)	180
	Number of Intervening Rows of Buildings	
Adjustments		No
		No
		No
		No

Source 2 Results

Leq(day):	53.8 dBA
Leq(night):	44.1 dBA
Ldn:	53.9 dBA
Incremental Ldn (Src 1-2):	59.3 dBA

Noise Source Parameters		Source 3
	Source Type:	Fixed Guideway
	Specific Source:	Rail Car
Daytime hrs	Avg. Number of Rail Cars/train	80
	Speed	30
	Avg. Number of Events/hr	0.75
Nighttime hrs	Avg. Number of Rail Cars/train	80
	Speed	30
	Avg. Number of Events/hr	0.08
Distance	Distance from Source to Receiver (ft)	180
	Number of Intervening Rows of Buildings	
Adjustments	Noise Barrier?	No
	Jointed Track?	No
	Embedded Track?	No
	Aerial Structure?	No

Source 3 Results

Leq(day):	51.4 dBA
Leq(night):	41.7 dBA
Ldn:	51.5 dBA
Incremental Ldn (Src 1-3):	60.0 dBA

Project:	South Glendale CP
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Noise Source Parameters	Number of Noise Sources: 3
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Noise Source Parameters		Source 1
	Source Type:	Fixed Guideway
	Specific Source:	Diesel Electric Locomotive
Daytime hrs	Avg. Number of Locos/train	1
	Speed (mph)	30
	Avg. Number of Events/hr	8.11
Nighttime hrs	Avg. Number of Locos/train	1
	Speed (mph)	30
	Avg. Number of Events/hr	0.89
Distance	Distance from Source to Receiver (ft)	235
	Number of Intervening Rows of Buildings	0
Adjustments		No
		No
		No
		No

Source 1 Results

Leq(day):	57.6 dBA
Leq(night):	48.0 dBA
Ldn:	57.8 dBA

Noise Source Parameters		Source 2
	Source Type:	Fixed Guideway
	Specific Source:	Diesel Electric Locomotive
Daytime hrs	Avg. Number of Locos/train	3
	Speed (mph)	30
	Avg. Number of Events/hr	1.13
Nighttime hrs	Avg. Number of Locos/train	3
	Speed (mph)	30
	Avg. Number of Events/hr	0.13
Distance	Distance from Source to Receiver (ft)	235
	Number of Intervening Rows of Buildings	
Adjustments		No
		No
		No
		No

Source 2 Results

Leq(day):	53.8 dBA
Leq(night):	44.4 dBA
Ldn:	54.1 dBA
Incremental Ldn (Src 1-2):	59.3 dBA

Noise Source Parameters		Source 3
	Source Type:	Fixed Guideway
	Specific Source:	Rail Car
Daytime hrs	Avg. Number of Rail Cars/train	80
	Speed	30
	Avg. Number of Events/hr	1.13
Nighttime hrs	Avg. Number of Rail Cars/train	80
	Speed	30
	Avg. Number of Events/hr	0.13
Distance	Distance from Source to Receiver (ft)	235
	Number of Intervening Rows of Buildings	
Adjustments	Noise Barrier?	No
	Jointed Track?	No
	Embedded Track?	No
	Aerial Structure?	No

Source 3 Results

Leq(day):	51.4 dBA
Leq(night):	42.1 dBA
Ldn:	51.7 dBA
Incremental Ldn (Src 1-3):	60.0 dBA

Attachment C – Traffic Data and TNM Input

SEGMENT	AM											PM												
	12	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8	9	10	11
Broadway e/o San Fernando Rd	45	21	12	11	34	80	189	344	415	430	430	495	611	561	560	568	601	723	595	427	293	204	146	73
Broadway e/o Pacific Ave	61	42	31	18	49	82	234	505	771	767	762	916	1,028	968	1,030	1,001	1,057	1,229	1,067	869	689	542	335	166
Broadway e/o Brand Blvd	90	70	49	34	60	117	346	735	1,080	1,080	1,146	1,054	1,004	977	1,050	998	1,132	1,299	1,205	1,124	755	638	304	158
Broadway e/o Glendale Ave	86	58	34	33	47	105	266	635	898	909	860	887	1,001	1,076	1,030	1,111	1,155	1,230	1,106	962	800	622	400	198
Broadway w/o Chevy Chase Dr	133	59	56	35	60	136	324	815	971	845	797	861	904	993	965	1,137	1,000	1,219	1,092	890	690	604	377	213
Broadway e/o Verdugo Rd	159	97	63	52	96	241	648	1,437	1,424	1,141	965	996	1,075	1,124	1,275	1,428	1,314	1,457	1,462	1,292	982	843	616	347
Colorado St e/o San Fernando Rd	65	43	35	24	56	130	308	643	620	563	558	609	637	640	698	647	692	760	591	481	368	323	212	179
Colorado St e/o Pacific Ave	253	154	102	69	151	364	584	1,247	1,550	1,549	1,603	1,737	1,813	1,472	1,903	1,770	1,854	1,750	2,041	1,884	1,516	1,288	923	557
Colorado St e/o Brand Blvd	257	124	81	58	105	270	486	1,142	1,315	1,188	1,344	1,440	1,570	1,550	1,579	1,621	1,686	1,832	1,722	1,488	1,222	1,078	751	450
Colorado St e/o Glendale Ave	236	104	75	62	67	155	406	884	1,128	1,086	1,270	1,411	1,533	1,507	1,578	1,610	1,633	1,745	1,669	1,460	1,250	1,108	752	419
Colorado St w/o Chevy Chase Dr	250	113	81	69	93	196	478	969	1,201	1,122	1,244	1,315	1,491	1,509	1,501	1,622	1,684	1,745	1,650	1,539	1,213	1,057	790	443
Colorado St e/o Verdugo Rd	196	114	55	73	109	280	611	1,151	1,301	1,127	1,208	1,307	1,434	1,361	1,464	1,726	1,625	1,787	1,678	1,510	1,037	922	620	343
Chevy Chase Dr e/o San Fernando Rd	103	63	35	41	51	166	424	837	1,011	747	778	876	933	940	910	1,048	1,068	1,055	977	798	622	453	334	213
Chevy Chase Dr e/o Brand Blvd	135	77	37	43	78	226	491	1,125	1,312	1,130	1,136	1,169	1,219	1,262	1,305	1,336	1,393	1,452	1,379	1,067	875	635	486	298
Chevy Chase Dr e/o Glendale Ave	168	70	58	64	81	200	552	1,167	1,282	1,078	1,092	1,214	1,186	1,316	1,278	1,395	1,467	1,598	1,546	1,155	926	736	501	341
Chevy Chase Dr w/o Adams St	134	62	50	31	52	135	430	1,127	1,143	919	807	893	978	931	1,051	1,184	1,155	1,254	1,163	906	669	540	413	208
Chevy Chase Dr n/o Acacia Ave	88	45	28	37	45	89	324	933	1,013	713	688	740	768	759	865	929	927	910	930	769	529	478	316	183
Chevy Chase Dr n/o Colorado St	143	78	45	49	57	126	416	1,179	1,266	1,011	1,016	1,066	1,194	1,174	1,174	1,446	1,388	1,606	1,394	1,153	859	756	481	270
Chevy Chase Dr n/o Broadway	96	49	31	29	34	77	261	839	872	677	651	659	755	774	905	1,025	954	1,001	978	858	674	523	331	161
Los Feliz Rd e/o San Fernando Rd	234	134	96	68	92	200	555	1,017	1,201	1,130	1,304	1,400	1,469	1,508	1,531	1,606	1,620	1,649	1,735	1,394	1,102	848	598	410
Los Feliz Rd e/o Brand Blvd	127	56	46	42	37	92	282	536	793	672	724	803	887	898	921	990	958	1,000	985	758	591	437	313	241
San Fernando Rd n/o Broadway	124	55	44	46	93	285	680	1,396	1,583	1,389	1,478	1,489	1,525	1,727	1,741	1,627	1,719	1,805	1,725	1,167	935	681	547	288
San Fernando Rd n/o Colorado St	196	108	59	48	65	149	406	789	822	903	1,022	1,390	1,574	1,719	1,700	1,783	1,962	2,000	1,707	1,097	739	650	474	344
San Fernando Rd n/o Chevy Chase Dr	220	99	69	69	126	370	950	1,799	1,958	1,616	1,618	1,704	1,778	1,822	1,861	2,084	2,115	2,122	1,866	1,394	1,061	790	582	383
San Fernando Rd n/o Los Feliz Rd	179	106	72	57	130	325	744	1,442	1,686	1,391	1,579	1,544	1,579	1,707	1,697	1,719	1,752	1,875	1,759	1,417	1,030	726	536	302
San Fernando Rd e/o Brand Blvd	305	200	137	144	203	420	877	1,542	1,688	1,790	1,785	1,844	1,954	1,918	1,940	2,075	2,163	2,189	2,050	1,645	1,319	1,101	867	622
Pacific Ave n/o Glenoaks Blvd	259	134	77	68	81	252	721	1,476	1,393	1,360	1,390	1,272	1,462	1,462	1,648	1,563	1,613	1,641	1,589	1,497	1,231	997	762	436
Pacific Ave n/o Lexington Dr	216	131	74	58	86	214	653	1,479	1,637	1,475	1,346	1,377	1,580	1,605	1,743	1,764	1,854	1,992	1,694	1,511	1,332	1,038	733	442
Pacific Ave n/o Broadway	163	109	62	49	66	170	541	1,207	1,343	1,204	1,157	1,195	1,366	1,387	1,452	1,442	1,528	1,676	1,474	1,267	1,077	850	571	348
Pacific Ave n/o Colorado St	184	97	76	66	99	240	689	1,660	1,791	1,464	1,370	1,320	1,471	1,667	1,595	1,606	1,698	1,923	1,812	1,369	1,046	853	590	394
Pacific Ave n/o San Fernando Rd	88	55	24	29	44	109	308	688	773	730	608	663	683	733	706	757	799	814	719	592	481	349	285	163
Brand Blvd n/o Glenoaks Blvd	149	55	43	30	50	173	374	830	1,024	986	979	1,061	1,072	1,103	1,066	1,205	1,124	1,276	1,252	1,091	860	657	459	269

SEGMENT	AM											PM												
	12	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8	9	10	11
Brand Blvd n/o Lexington Dr	212	90	85	45	103	239	576	1,039	1,288	1,366	1,459	1,664	1,822	1,792	1,725	1,666	1,635	1,711	1,785	1,606	1,373	1,139	859	441
Brand Blvd n/o Broadway	170	86	62	35	71	180	429	845	1,005	1,102	1,175	1,372	1,422	1,373	1,444	1,368	1,403	1,543	1,435	1,373	1,141	967	620	296
Brand Blvd n/o Colorado St	209	86	50	42	69	160	445	917	1,051	1,173	1,155	1,405	1,583	1,686	1,559	1,673	1,780	1,879	1,697	1,530	1,276	1,109	718	342
Brand Blvd n/o Chevy Chase Dr	146	88	49	41	71	151	486	1,385	1,429	1,278	1,315	1,368	1,447	1,525	1,621	1,697	1,621	1,740	1,496	1,180	844	691	405	213
Brand Blvd n/o Los Feliz Rd	142	85	63	36	57	171	627	1,451	1,790	1,489	1,333	1,410	1,544	1,529	1,652	1,703	1,817	1,925	1,712	1,262	882	727	483	259
Brand Blvd n/o San Fernando Rd	156	93	58	53	68	174	566	1,143	1,366	1,141	1,142	1,166	1,277	1,342	1,370	1,506	1,694	1,846	1,642	1,333	957	741	564	336
Glendale Ave n/o Monterey Rd	142	94	38	43	62	225	764	1,790	2,156	1,757	1,786	1,628	1,879	1,827	1,731	2,045	1,948	2,062	2,079	1,562	1,266	1,163	728	314
Glendale Ave n/o Lexington Dr	257	150	90	69	135	331	858	1,949	2,082	1,937	2,042	2,266	2,509	2,463	2,340	2,421	2,344	2,576	2,496	2,206	1,669	1,473	848	514
Glendale Ave n/o Broadway	190	100	65	48	64	173	499	1,243	1,441	1,350	1,589	1,723	1,849	1,939	1,871	1,887	1,852	1,877	1,882	1,526	1,339	1,018	643	337
Glendale Ave n/o Colorado St	186	98	55	42	60	145	414	1,055	1,208	1,146	1,387	1,399	1,643	1,685	1,579	1,617	1,667	1,774	1,617	1,417	1,166	887	631	304
Glendale Ave n/o Chevy Chase Dr	166	86	59	44	66	165	459	1,033	1,140	1,070	1,179	1,251	1,343	1,377	1,377	1,395	1,385	1,572	1,429	1,150	848	644	458	304
Glendale Ave n/o Los Feliz Rd	176	106	70	81	103	253	731	1,382	1,620	1,319	1,266	1,368	1,508	1,461	1,449	1,564	1,655	1,926	1,781	1,335	993	739	519	380
Glendale Ave n/o San Fernando Rd	152	76	60	62	113	260	492	967	979	791	782	793	808	777	933	822	970	1,085	986	769	627	499	352	231
York Blvd e/o Verdugo Rd	79	61	32	30	45	142	492	1,190	1,169	915	603	609	617	632	779	801	843	969	906	690	534	413	326	157
SR 134 WB AT PACIFIC	960	580	484	521	1,226	3,629	7,063	8,500	8,406	7,685	6,687	6,235	6,356	6,183	6,488	6,853	7,025	7,127	6,402	5,170	4,258	3,954	2,860	1,706
SR 134 EB AT PACIFIC	1,026	596	429	390	602	1,439	3,437	5,915	5,882	5,164	5,099	5,208	5,662	6,055	6,567	7,066	7,281	7,313	7,414	6,378	4,676	3,842	3,049	1,922
SR 134 WB AT CENTRAL	836	512	437	477	1,151	3,465	6,685	8,411	8,498	7,653	6,279	5,617	5,596	5,367	5,632	5,932	5,972	6,230	5,427	4,320	3,584	3,349	2,435	1,453
SR 134 EB AT BRAND	1,123	655	464	416	655	1,588	3,816	6,709	6,679	5,876	5,738	5,870	6,371	6,831	7,503	8,122	8,456	8,565	8,575	7,128	5,294	4,305	3,420	2,145
SR 134 WB AT GLENDALE	875	525	439	493	1,257	3,829	7,362	9,458	9,110	8,461	7,007	6,279	6,176	5,997	6,212	6,596	6,652	7,057	6,204	4,824	3,827	3,451	2,528	1,528
SR 134 EB AT GLENDALE	1,191	727	535	484	729	1,727	4,032	6,921	6,911	6,156	5,997	6,336	6,827	7,335	8,019	8,759	9,023	9,069	8,983	7,602	5,637	4,674	3,647	2,280
SR 2 WB N/O YORK BLVD	673	507	473	508	882	2,519	5,661	5,472	4,862	4,881	4,111	3,634	3,679	3,646	3,780	4,570	4,732	5,005	4,337	3,299	2,555	2,294	1,714	1,098
SR 2 EB N/O YORK BLVD	854	466	366	306	486	1,137	2,561	4,420	4,453	3,546	3,313	3,340	3,566	3,977	4,795	6,092	7,346	7,847	7,335	5,395	3,608	3,030	2,607	1,562
SR 2 WB AT YORK BLVD / DELEVAN	1,231	1,051	1,017	1,067	1,492	3,131	5,543	5,149	4,837	4,980	4,495	4,140	4,277	4,042	4,149	4,684	4,714	5,010	4,500	3,668	3,019	2,783	2,231	1,620
SR 2 EB AT YORK BLVD / DELEVAN	1,240	959	881	832	900	1,274	2,293	3,639	3,653	2,973	2,892	2,994	3,331	3,621	4,401	5,911	7,267	7,789	7,246	5,137	3,392	2,940	2,657	1,782
SR 2 WB AT SAN FERNANDO RD	518	482	484	502	816	2,780	6,010	5,145	5,137	5,292	4,475	3,887	3,894	3,745	3,846	4,420	4,505	4,928	4,478	3,220	2,548	2,323	1,698	981
SR 2 EB AT SAN FERNANDO RD	802	448	351	262	345	844	2,017	3,345	3,360	2,740	2,736	2,851	3,155	3,511	4,267	5,505	6,711	7,320	6,943	5,296	3,661	3,082	2,745	1,553

Roadway Segment	Details		Hourly	Period	Type	Volume	Speed	
Brand Blvd n/o Lexington Dr	Road Width:	90	1,578	Day	Auto	1515	30	
	Road Y Coord:	45			MT	32	30	
	Mix				HT	32	30	
		MT	2%	1,372	Evening	Auto	1317	30
		HT	2%			MT	27	30
						HT	27	30
				294	Night	Auto	282	30
						MT	6	30
						HT	6	30
			Fut:	1,652	Day	Auto	1586	30
						MT	33	30
						HT	33	30
				1,436	Evening	Auto	1378	30
						MT	29	30
				HT		29	30	
			308	Night	Auto	296	30	
					MT	6	30	
					HT	6	30	
Brand Blvd n/o Broadway	Road Width:	90	1,290	Day	Auto	1238	30	
	Road Y Coord:	45			MT	26	30	
	Mix				HT	26	30	
		MT	2%	1,159	Evening	Auto	1113	30
		HT	2%			MT	23	30
						HT	23	30
				216	Night	Auto	208	30
						MT	4	30
						HT	4	30
			Fut:	1,438	Day	Auto	1380	30
						MT	29	30
						HT	29	30
				1,293	Evening	Auto	1241	30
						MT	26	30
				HT		26	30	
			241	Night	Auto	232	30	
					MT	5	30	
					HT	5	30	
Brand Blvd n/o Colorado St	Road Width:	90	1,464	Day	Auto	1405	30	
	Road Y Coord:	45			MT	29	30	
	Mix				HT	29	30	
		MT	2%	1,305	Evening	Auto	1253	30
		HT	2%			MT	26	30
						HT	26	30
				236	Night	Auto	226	30
						MT	5	30
						HT	5	30
			Fut:	1,550	Day	Auto	1488	30
						MT	31	30
						HT	31	30
				1,383	Evening	Auto	1327	30
						MT	28	30
				HT		28	30	
			250	Night	Auto	240	30	
					MT	5	30	
					HT	5	30	

Roadway Segment	Details		Hourly	Period	Type	Volume	Speed	
Brand Blvd n/o Chevy Chase Dr	Road Width:	90	1,494	Day	Auto	1435	30	
	Road Y Coord:	45			MT	30	30	
	Mix				HT	30	30	
		MT	2%	906	Evening	Auto	869	30
		HT	2%			MT	18	30
						HT	18	30
				183	Night	Auto	176	30
						MT	4	30
						HT	4	30
			Fut:	1,803	Day	Auto	1731	30
						MT	36	30
						HT	36	30
			1,092	Evening	Auto	1049	30	
					MT	22	30	
					HT	22	30	
			221	Night	Auto	212	30	
					MT	4	30	
					HT	4	30	
Brand Blvd n/o Los Feliz Rd	Road Width:	90	1,610	Day	Auto	1545	30	
	Road Y Coord:	45			MT	32	30	
	Mix				HT	32	30	
		MT	2%	955	Evening	Auto	917	30
		HT	2%			MT	19	30
						HT	19	30
				213	Night	Auto	205	30
						MT	4	30
						HT	4	30
			Fut:	1,930	Day	Auto	1853	30
						MT	39	30
						HT	39	30
			1,145	Evening	Auto	1099	30	
					MT	23	30	
					HT	23	30	
			256	Night	Auto	245	30	
					MT	5	30	
					HT	5	30	
Brand Blvd n/o San Fernando Rd	Road Width:	100	1,384	Day	Auto	1329	30	
	Road Y Coord:	50			MT	28	30	
	Mix				HT	28	30	
		MT	2%	1,009	Evening	Auto	968	30
		HT	2%			MT	20	30
						HT	20	30
				229	Night	Auto	220	30
						MT	5	30
						HT	5	30
			Fut:	1,716	Day	Auto	1647	30
						MT	34	30
						HT	34	30
			1,250	Evening	Auto	1200	30	
					MT	25	30	
					HT	25	30	
			284	Night	Auto	273	30	
					MT	6	30	
					HT	6	30	

Roadway Segment	Details		Hourly Period	Type	Volume	Speed		
Broadway e/o San Fernando Rd	Road Width:	50	530	Day	Auto	509	35	
	Road Y Coord:	25			MT	11	35	
	Mix				HT	11	35	
		MT	2%	309	Evening	Auto	297	35
		HT	2%			MT	6	35
						HT	6	35
				68	Night	Auto	65	35
						MT	1	35
						HT	1	35
			Fut:	651	Day	Auto	625	35
						MT	13	35
						HT	13	35
			380	Evening	Auto	365	35	
					MT	8	35	
					HT	8	35	
			84	Night	Auto	80	35	
					MT	2	35	
					HT	2	35	
Broadway e/o Pacific Ave	Road Width:	50	924	Day	Auto	887	35	
	Road Y Coord:	25			MT	18	35	
	Mix				HT	18	35	
		MT	2%	699	Evening	Auto	671	35
		HT	2%			MT	14	35
						HT	14	35
				113	Night	Auto	108	35
						MT	2	35
						HT	2	35
			Fut:	1,054	Day	Auto	1012	35
						MT	21	35
						HT	21	35
			798	Evening	Auto	766	35	
					MT	16	35	
					HT	16	35	
			129	Night	Auto	124	35	
					MT	3	35	
					HT	3	35	
Broadway e/o Brand Blvd	Road Width:	50	1,063	Day	Auto	1020	35	
	Road Y Coord:	25			MT	21	35	
	Mix				HT	21	35	
		MT	2%	839	Evening	Auto	805	35
		HT	2%			MT	17	35
						HT	17	35
				136	Night	Auto	131	35
						MT	3	35
						HT	3	35
			Fut:	1,050	Day	Auto	1008	35
						MT	21	35
						HT	21	35
			829	Evening	Auto	795	35	
					MT	17	35	
					HT	17	35	
			135	Night	Auto	129	35	
					MT	3	35	
					HT	3	35	

Roadway Segment	Details		Hourly Period	Type	Volume	Speed	
Broadway e/o Glendale Ave	Road Width:	50	991	Day	Auto	951	35
	Road Y Coord:	25			MT	20	35
	Mix				HT	20	35
	MT	2%	794	Evening	Auto	762	35
	HT	2%			MT	16	35
					HT	16	35
			136	Night	Auto	131	35
					MT	3	35
					HT	3	35
			Fut: 1,272	Day	Auto	1221	35
					MT	25	35
					HT	25	35
			1,020	Evening	Auto	979	35
					MT	20	35
					HT	20	35
		175	Night	Auto	168	35	
				MT	3	35	
				HT	3	35	
Broadway e/o Verdugo Rd	Road Width:	50	1,256	Day	Auto	1206	35
	Road Y Coord:	25			MT	25	35
	Mix				HT	25	35
	MT	2%	1,037	Evening	Auto	996	35
	HT	2%			MT	21	35
					HT	21	35
			257	Night	Auto	247	35
					MT	5	35
					HT	5	35
			Fut: 1,397	Day	Auto	1341	35
					MT	28	35
					HT	28	35
			1,154	Evening	Auto	1108	35
					MT	23	35
					HT	23	35
		286	Night	Auto	275	35	
				MT	6	35	
				HT	6	35	
Chevy Chase Dr e/o San Fernando Rd	Road Width:	50	933	Day	Auto	895	35
	Road Y Coord:	25			MT	19	35
	Mix				HT	19	35
	MT	2%	625	Evening	Auto	600	35
	HT	2%			MT	13	35
					HT	13	35
			159	Night	Auto	153	35
					MT	3	35
					HT	3	35
			Fut: 1,023	Day	Auto	982	35
					MT	20	35
					HT	20	35
			685	Evening	Auto	658	35
					MT	14	35
					HT	14	35
		174	Night	Auto	167	35	
				MT	3	35	
				HT	3	35	

Roadway Segment	Details		Hourly	Period	Type	Volume	Speed
Chevy Chase Dr e/o Brand Blvd	Road Width:	50	1,270	Day	Auto	1220	35
	Road Y Coord:	25			MT	25	35
	Mix				HT	25	35
	MT	2%	860	Evening	Auto	826	35
	HT	2%			MT	17	35
					HT	17	35
			208	Night	Auto	200	35
					MT	4	35
					HT	4	35
			Fut: 1,515	Day	Auto	1455	35
					MT	30	35
					HT	30	35
			1,026	Evening	Auto	985	35
					MT	21	35
			HT		21	35	
		248	Night	Auto	238	35	
				MT	5	35	
				HT	5	35	
Chevy Chase Dr e/o Glendale Ave	Road Width:	50	1,303	Day	Auto	1251	35
	Road Y Coord:	25			MT	26	35
	Mix				HT	26	35
	MT	2%	940	Evening	Auto	903	35
	HT	2%			MT	19	35
					HT	19	35
			226	Night	Auto	217	35
					MT	5	35
					HT	5	35
			Fut: 1,456	Day	Auto	1398	35
					MT	29	35
					HT	29	35
			1,050	Evening	Auto	1008	35
					MT	21	35
			HT		21	35	
		253	Night	Auto	243	35	
				MT	5	35	
				HT	5	35	
Chevy Chase Dr n/o Acacia Ave	Road Width:	60	848	Day	Auto	814	35
	Road Y Coord:	30			MT	17	35
	Mix				HT	17	35
	MT	2%	592	Evening	Auto	568	35
	HT	2%			MT	12	35
					HT	12	35
			128	Night	Auto	123	35
					MT	3	35
					HT	3	35
			Fut: 569	Day	Auto	547	35
					MT	11	35
					HT	11	35
			397	Evening	Auto	382	35
					MT	8	35
			HT		8	35	
		86	Night	Auto	83	35	
				MT	2	35	
				HT	2	35	

Roadway Segment	Details		Hourly Period	Type	Volume	Speed	
Chevy Chase Dr n/o Colorado St	Road Width:	60	1,240	Day	Auto	1190	35
	Road Y Coord:	30			MT	25	35
	Mix				HT	25	35
	MT	2%	920	Evening	Auto	884	35
	HT	2%			MT	18	35
					HT	18	35
			185	Night	Auto	177	35
					MT	4	35
					HT	4	35
			938	Day	Auto	900	35
					MT	19	35
					HT	19	35
			696	Evening	Auto	668	35
					MT	14	35
		HT			14	35	
		140	Night	Auto	134	35	
				MT	3	35	
				HT	3	35	
Chevy Chase Dr n/o Broadway	Road Width:	60	840	Day	Auto	806	35
	Road Y Coord:	30			MT	17	35
	Mix				HT	17	35
	MT	2%	684	Evening	Auto	657	35
	HT	2%			MT	14	35
					HT	14	35
			119	Night	Auto	114	35
					MT	2	35
					HT	2	35
			757	Day	Auto	727	35
					MT	15	35
					HT	15	35
			617	Evening	Auto	592	35
					MT	12	35
		HT			12	35	
		107	Night	Auto	103	35	
				MT	2	35	
				HT	2	35	
Colorado St e/o San Fernando Rd	Road Width:	60	639	Day	Auto	614	35
	Road Y Coord:	30			MT	13	35
	Mix				HT	13	35
	MT	2%	391	Evening	Auto	376	35
	HT	2%			MT	8	35
					HT	8	35
			117	Night	Auto	112	35
					MT	2	35
					HT	2	35
			788	Day	Auto	756	35
					MT	16	35
					HT	16	35
			482	Evening	Auto	463	35
					MT	10	35
		HT			10	35	
		144	Night	Auto	139	35	
				MT	3	35	
				HT	3	35	

Roadway Segment	Details		Hourly Period	Type	Volume	Speed	
Colorado St e/o Pacific Ave	Road Width:	70	1,689	Day	Auto	1621	35
	Road Y Coord:	35			MT	34	35
	Mix				HT	34	35
	MT	2%	1,561	Evening	Auto	1498	35
	HT	2%			MT	31	35
					HT	31	35
			350	Night	Auto	336	35
					MT	7	35
					HT	7	35
		Fut:	1,971	Day	Auto	1892	35
					MT	39	35
					HT	39	35
			1,822	Evening	Auto	1749	35
					MT	36	35
			HT		36	35	
		409	Night	Auto	393	35	
				MT	8	35	
				HT	8	35	
Colorado St e/o Brand Blvd	Road Width:	60	1,502	Day	Auto	1442	35
	Road Y Coord:	30			MT	30	35
	Mix				HT	30	35
	MT	2%	1,265	Evening	Auto	1214	35
	HT	2%			MT	25	35
					HT	25	35
			287	Night	Auto	276	35
					MT	6	35
					HT	6	35
		Fut:	1,846	Day	Auto	1772	35
					MT	37	35
					HT	37	35
			1,555	Evening	Auto	1493	35
					MT	31	35
			HT		31	35	
		353	Night	Auto	339	35	
				MT	7	35	
				HT	7	35	
Colorado St e/o Glendale Ave	Road Width:	60	1,418	Day	Auto	1361	35
	Road Y Coord:	30			MT	28	35
	Mix				HT	28	35
	MT	2%	1,270	Evening	Auto	1219	35
	HT	2%			MT	25	35
					HT	25	35
			252	Night	Auto	242	35
					MT	5	35
					HT	5	35
		Fut:	1,682	Day	Auto	1615	35
					MT	34	35
					HT	34	35
			1,506	Evening	Auto	1446	35
					MT	30	35
			HT		30	35	
		299	Night	Auto	287	35	
				MT	6	35	
				HT	6	35	

Roadway Segment	Details		Hourly	Period	Type	Volume	Speed
Colorado St e/o Verdugo Rd	Road Width:	60	1,428	Day	Auto	1371	35
	Road Y Coord:	30			MT	29	35
	Mix				HT	29	35
	MT	2%	1,154	Evening	Auto	1108	35
	HT	2%			MT	23	35
					HT	23	35
			266	Night	Auto	256	35
					MT	5	35
					HT	5	35
			Fut: 1,627	Day	Auto	1562	35
					MT	33	35
					HT	33	35
		1,315	Evening	Auto	1262	35	
				MT	26	35	
				HT	26	35	
		303	Night	Auto	291	35	
				MT	6	35	
				HT	6	35	
Glendale Ave n/o Lexington Dr	Road Width:	70	2,284	Day	Auto	2192	30
	Road Y Coord:	35			MT	46	30
	Mix				HT	46	30
	MT	2%	1,781	Evening	Auto	1710	30
	HT	2%			MT	36	30
					HT	36	30
			361	Night	Auto	347	30
					MT	7	30
					HT	7	30
			Fut: 2,328	Day	Auto	2235	30
					MT	47	30
					HT	47	30
		1,816	Evening	Auto	1743	30	
				MT	36	30	
				HT	36	30	
		368	Night	Auto	353	30	
				MT	7	30	
				HT	7	30	
Glendale Ave n/o Broadway	Road Width:	70	1,708	Day	Auto	1640	30
	Road Y Coord:	35			MT	34	30
	Mix				HT	34	30
	MT	2%	1,294	Evening	Auto	1242	30
	HT	2%			MT	26	30
					HT	26	30
			235	Night	Auto	226	30
					MT	5	30
					HT	5	30
			Fut: 1,889	Day	Auto	1813	30
					MT	38	30
					HT	38	30
		1,431	Evening	Auto	1374	30	
				MT	29	30	
				HT	29	30	
		260	Night	Auto	250	30	
				MT	5	30	
				HT	5	30	

Roadway Segment	Details		Hourly Period	Type	Volume	Speed	
Glendale Ave n/o Colorado St	Road Width:	70	1,483	Day	Auto	1423	30
	Road Y Coord:	35			MT	30	30
	Mix				HT	30	30
	MT	2%	1,158	Evening	Auto	1111	30
	HT	2%			MT	23	30
					HT	23	30
			215	Night	Auto	207	30
					MT	4	30
					HT	4	30
			Fut: 1,930	Day	Auto	1853	30
					MT	39	30
					HT	39	30
		1,507	Evening	Auto	1447	30	
				MT	30	30	
				HT	30	30	
		280	Night	Auto	269	30	
				MT	6	30	
				HT	6	30	
Glendale Ave n/o Chevy Chase Dr	Road Width:	60	1,296	Day	Auto	1244	30
	Road Y Coord:	30			MT	26	30
	Mix				HT	26	30
	MT	2%	881	Evening	Auto	845	30
	HT	2%			MT	18	30
					HT	18	30
			201	Night	Auto	193	30
					MT	4	30
					HT	4	30
			Fut: 1,659	Day	Auto	1592	30
					MT	33	30
					HT	33	30
		1,127	Evening	Auto	1082	30	
				MT	23	30	
				HT	23	30	
		257	Night	Auto	247	30	
				MT	5	30	
				HT	5	30	
Glendale Ave n/o Los Feliz Rd	Road Width:	60	1,526	Day	Auto	1465	30
	Road Y Coord:	30			MT	31	30
	Mix				HT	31	30
	MT	2%	1,023	Evening	Auto	982	30
	HT	2%			MT	20	30
					HT	20	30
			269	Night	Auto	258	30
					MT	5	30
					HT	5	30
			Fut: 1,808	Day	Auto	1736	30
					MT	36	30
					HT	36	30
		1,212	Evening	Auto	1164	30	
				MT	24	30	
				HT	24	30	
		319	Night	Auto	306	30	
				MT	6	30	
				HT	6	30	

Roadway Segment	Details		Hourly Period	Type	Volume	Speed	
Glendale Ave n/o San Fernando Rd	Road Width:	50	892	Day	Auto	856	30
	Road Y Coord:	25			MT	18	30
	Mix				HT	18	30
	MT	2%	632	Evening	Auto	607	30
	HT	2%			MT	13	30
					HT	13	30
			200	Night	Auto	192	30
					MT	4	30
					HT	4	30
			Fut: 1,288	Day	Auto	1237	30
					MT	26	30
					HT	26	30
			913	Evening	Auto	877	30
					MT	18	30
			HT		18	30	
		289	Night	Auto	277	30	
				MT	6	30	
				HT	6	30	
Pacific Ave n/o Lexington Dr	Road Width:	50	1,627	Day	Auto	1562	30
	Road Y Coord:	25			MT	33	30
	Mix				HT	33	30
	MT	2%	1,292	Evening	Auto	1240	30
	HT	2%			MT	26	30
					HT	26	30
			289	Night	Auto	278	30
					MT	6	30
					HT	6	30
			Fut: 1,802	Day	Auto	1730	30
					MT	36	30
					HT	36	30
			1,431	Evening	Auto	1374	30
					MT	29	30
			HT		29	30	
		320	Night	Auto	308	30	
				MT	6	30	
				HT	6	30	
Pacific Ave n/o Broadway	Road Width:	50	1,369	Day	Auto	1314	30
	Road Y Coord:	25			MT	27	30
	Mix				HT	27	30
	MT	2%	1,064	Evening	Auto	1022	30
	HT	2%			MT	21	30
					HT	21	30
			231	Night	Auto	222	30
					MT	5	30
					HT	5	30
			Fut: 1,558	Day	Auto	1496	30
					MT	31	30
					HT	31	30
			1,212	Evening	Auto	1163	30
					MT	24	30
			HT		24	30	
		263	Night	Auto	252	30	
				MT	5	30	
				HT	5	30	

Roadway Segment	Details		Hourly Period	Type	Volume	Speed	
Pacific Ave n/o Colorado St	Road Width:	50	1,616	Day	Auto	1551	30
	Road Y Coord:	25			MT	32	30
	Mix				HT	32	30
	MT	2%	1,090	Evening	Auto	1047	30
	HT	2%			MT	22	30
					HT	22	30
			271	Night	Auto	260	30
					MT	5	30
					HT	5	30
			Fut: 1,764	Day	Auto	1694	30
					MT	35	30
					HT	35	30
			1,190	Evening	Auto	1142	30
					MT	24	30
			HT		24	30	
		296	Night	Auto	284	30	
				MT	6	30	
				HT	6	30	
Pacific Ave n/o San Fernando Rd	Road Width:	50	723	Day	Auto	694	30
	Road Y Coord:	25			MT	14	30
	Mix				HT	14	30
	MT	2%	474	Evening	Auto	455	30
	HT	2%			MT	9	30
					HT	9	30
			123	Night	Auto	118	30
					MT	2	30
					HT	2	30
			Fut: 742	Day	Auto	712	30
					MT	15	30
					HT	15	30
			487	Evening	Auto	467	30
					MT	10	30
			HT		10	30	
		126	Night	Auto	121	30	
				MT	3	30	
				HT	3	30	
San Fernando Rd n/o Broadway	Road Width:	60	1,597	Day	Auto	1524	35
	Road Y Coord:	30			MT	24	35
	Mix				HT	49	35
	MT	2%	926	Evening	Auto	879	35
	HT	3%			MT	19	35
					HT	28	35
			240	Night	Auto	229	35
					MT	4	35
					HT	7	35
			Fut: 1,743	Day	Auto	1663	35
					MT	27	35
					HT	53	35
			1,010	Evening	Auto	964	35
					MT	15	35
			HT		31	35	
		262	Night	Auto	250	35	
				MT	4	35	
				HT	8	35	

Roadway Segment	Details		Hourly	Period	Type	Volume	Speed
San Fernando Rd n/o Colorado St	Road Width:	60	1,447	Day	Auto	1381	35
	Road Y Coord:	30			MT	22	35
	Mix				HT	44	35
	MT	2%	828	Evening	Auto	787	35
	HT	3%			MT	17	35
					HT	25	35
			205	Night	Auto	196	35
					MT	3	35
					HT	6	35
			Fut: 1,701	Day	Auto	1623	35
					MT	26	35
					HT	52	35
			974	Evening	Auto	929	35
					MT	15	35
			HT		30	35	
		241	Night	Auto	230	35	
				MT	4	35	
				HT	7	35	
San Fernando Rd n/o Chevy Chase Dr	Road Width:	28	1,865	Day	Auto	1779	35
	Road Y Coord:	14			MT	28	35
	Mix				HT	57	35
	MT	2%	1,083	Evening	Auto	1029	35
	HT	3%			MT	22	35
					HT	33	35
			319	Night	Auto	305	35
					MT	5	35
					HT	10	35
			Fut: 2,356	Day	Auto	2248	35
					MT	36	35
					HT	72	35
			1,368	Evening	Auto	1306	35
					MT	21	35
			HT		42	35	
		403	Night	Auto	385	35	
				MT	6	35	
				HT	12	35	
San Fernando Rd n/o Los Feliz Rd	Road Width:	65	1,647	Day	Auto	1572	35
	Road Y Coord:	32.5			MT	25	35
	Mix				HT	50	35
	MT	2%	1,060	Evening	Auto	1006	35
	HT	3%			MT	21	35
					HT	32	35
			273	Night	Auto	260	35
					MT	4	35
					HT	8	35
			Fut: 2,166	Day	Auto	2067	35
					MT	33	35
					HT	66	35
			1,393	Evening	Auto	1329	35
					MT	21	35
			HT		43	35	
		359	Night	Auto	342	35	
				MT	5	35	
				HT	11	35	

Roadway Segment	Details		Hourly Period	Type	Volume	Speed		
San Fernando Rd e/o Brand Blvd	Road Width:	65	1,913	Day	Auto	1825	35	
	Road Y Coord:	32.5			MT	29	35	
	Mix				HT	58	35	
		MT	2%	1,356	Evening	Auto	1287	35
		HT	3%			MT	27	35
						HT	41	35
				420	Night	Auto	401	35
						MT	6	35
						HT	13	35
			Fut:	2,441	Day	Auto	2329	35
						MT	37	35
						HT	75	35
				1,730	Evening	Auto	1651	35
						MT	26	35
			HT			53	35	
			536	Night	Auto	511	35	
					MT	8	35	
					HT	16	35	
York Blvd e/o Verdugo Rd	Road Width:	35	834	Day	Auto	801	25	
	Road Y Coord:	17.5			MT	17	25	
	Mix				HT	17	25	
		MT	2%	544	Evening	Auto	522	25
		HT	2%			MT	11	25
						HT	11	25
				151	Night	Auto	145	25
						MT	3	25
						HT	3	25
			Fut:	885	Day	Auto	850	25
						MT	18	25
						HT	18	25
				578	Evening	Auto	555	25
						MT	12	25
			HT			12	25	
			160	Night	Auto	154	25	
					MT	3	25	
					HT	3	25	
SR 134 AT PACIFIC	Road Width:	140	13,220	Day	Auto	12448	65	
	Road Y Coord:	70			MT	427	65	
	Mix				HT	346	65	
		MT	3%	9,498	Evening	Auto	9060	65
		HT	3%			MT	190	65
						HT	248	65
				3,518	Night	Auto	3312	65
						MT	114	65
						HT	92	65
			Fut:	14,091	Day	Auto	13267	65
						MT	455	65
						HT	369	65
				10,123	Evening	Auto	9531	65
						MT	327	65
			HT			265	65	
			3,749	Night	Auto	3530	65	
					MT	121	65	
					HT	98	65	

Roadway Segment	Details		Hourly	Period	Type	Volume	Speed	
SR 134 AT CENTRAL/BRAND	Road Width:	140	13,488	Day	Auto	12700	65	
	Road Y Coord:	70			MT	436	65	
	Mix				HT	353	65	
	MT	3%	9,258	Evening	Auto	8831	65	
	HT	3%			MT	185	65	
					HT	242	65	
				3,552	Night	Auto	3344	65
						MT	115	65
						HT	93	65
			Fut:	14,468	Day	Auto	13622	65
						MT	467	65
						HT	378	65
				9,931	Evening	Auto	9350	65
						MT	321	65
				HT		260	65	
			3,810	Night	Auto	3587	65	
					MT	123	65	
					HT	100	65	
SR 134 AT GLENDALE	Road Width:	140	14,627	Day	Auto	13772	65	
	Road Y Coord:	70			MT	473	65	
	Mix				HT	383	65	
	MT	3%	9,952	Evening	Auto	9493	65	
	HT	3%			MT	199	65	
					HT	260	65	
				3,814	Night	Auto	3591	65
						MT	123	65
						HT	100	65
			Fut:	15,664	Day	Auto	14748	65
						MT	506	65
						HT	410	65
				10,658	Evening	Auto	10035	65
						MT	344	65
				HT		279	65	
			4,084	Night	Auto	3845	65	
					MT	132	65	
					HT	107	65	
SR 2 AT YORK BLVD / DELEVAN	Road Width:	180	9,226	Day	Auto	8829	65	
	Road Y Coord:	90			MT	351	65	
	Mix				HT	46	65	
	MT	4%	6,992	Evening	Auto	6817	65	
	HT	1%			MT	140	65	
					HT	35	65	
				3,456	Night	Auto	3307	65
						MT	132	65
						HT	17	65
			Fut:	9,470	Day	Auto	9062	65
						MT	361	65
						HT	47	65
				7,177	Evening	Auto	6867	65
						MT	273	65
				HT		36	65	
			3,548	Night	Auto	3395	65	
					MT	135	65	
					HT	18	65	